CE407 SEPARATIONS

Lecture 15b

Instructor: David Courtemanche

University at Buffalo Department of Chemical
and Biological Engineering
school of Engineering and Applied Sciences

Multi-Stage Cross Current LLE

- Consider a countercurrent liquid extraction process. The 8000 kg/hr feed (L_0) stream comprises 8 mass % lactic acid (solute C) and 92 mass % water (diluent A). The 25,000 kg/hr entering solvent (V_{N+1}) stream is pure nonanol (solvent \bm{B}). The exiting raffinate should have 0.5 mass % lactic acid on a nonanol-free basis.
- What will be the flow rate of the exiting extract?
- What will be the composition of the exiting extract on a water-free basis?
- Note: the location of the Mixing point will make doing mass balances on the C component will be difficult – do mass balances on the B component instead.

Multi-Stage Cross Current LLE

Figure 3: Phase diagram quantifying liquid-liquid equilibria of ternary mixtures of water (diluent, A), nonanol (solvent, B) and lactic acid (solute, C)

n

1 hour basis A (diluent) = water B (solvent) = nonanol C (solute) = lactic acid

- Start by calculating the fictitious mixture point
- $M =$ the rate at which liquid enters the system $= L_0 + V_{N+1} = 33,000 kg$

•
$$
\begin{aligned}\n\mathbf{x}_M &= (\mathbf{x}_c)_M = \frac{\mathbf{x}_0 L_0 + \mathbf{y}_{N+1} V_{N+1}}{L_0 + V_{N+1}} \\
\mathbf{x}_M &= (\mathbf{x}_c)_M = \frac{0.08 \times 8000 + 0 \times 25,000}{8000 + 25,000} = 0.0194 \\
\mathbf{x}_M &= (\mathbf{x}_B)_M = \frac{(\mathbf{x}_B)_0 L_0 + (\mathbf{y}_B)_{N+1} V_{N+1}}{L_0 + V_{N+1}} = \frac{0 \times 8000 + 1 \times 25,000}{8000 + 25,000} = 0.7576\n\end{aligned}
$$

- \bullet Locate *M* as a point on the line $\overline{L_0 V_{N+1}}$ where $x_M = (x_c)_M =$ 0.0194 or $(x_B)_M = 0.7576$
- Because the left -hand side of the two phase boundary is essential at $x_B =$ **0**, we can state that $L_N \approx L'_N =$ 0.005
- M is also equal to the rate at which liquid exits the system and therefore lies on the line $\overline{L_N \, V_1}$
- We can extend the line $\overline{L_N V_M}$ to reach the two -phase boundary in order to locate V_1
- $(y_B)_1 = 0$. 94 and $(y_c)_1 = 0$. 022

- Working with Solute Mass Fractions:
- \bullet $\frac{V_1}{I}$ $\bm{L_N}$ $=\frac{x_M-x_N}{\sqrt{2}}$ $y_1 - x_M$ $=\frac{0.0194 - 0.005}{0.033 - 0.0104}$ 0.022-0.0194 $= 5.54$

•
$$
L_N = \frac{M}{1 + {V_1}_{/L_N}} = \frac{33,000}{1 + 5.54} = 5045 kg
$$

•
$$
V_1 = M - L_N = 33,000 - 5045 = 27,955 kg
$$

• Working with Solvent Mass Fractions:

•
$$
\frac{V_1}{L_N} = \frac{(x_B)_M - (x_B)_N}{(y_B)_1 - (x_B)_M} = \frac{0.7576 - 0}{0.94 - 0.7576} = 4.15
$$

•
$$
L_N = \frac{M}{1 + {V_1}_{L_N}} = \frac{33,000}{1 + 4.15} = 6403 kg
$$

•
$$
V_1 = M - L_N = 33,000 - 6403 = 26,597 kg
$$

Small errors in reading the graph will have much less effect on the B balance answer. The second set of values is more reliable.

- $V_1 = 26,597 kg$
- $(y_B)_1 = 0.94$ and $(y_c)_1 = 0.022$
- $(y_c)_1|_{water-free} = \frac{0.022}{0.94+0.022} = 0.023$
- $(y_B)_1|_{water-free} = \frac{0.94}{0.94 + 0.022} = 0.977$
-
- One could also read V_1' off of the graph

