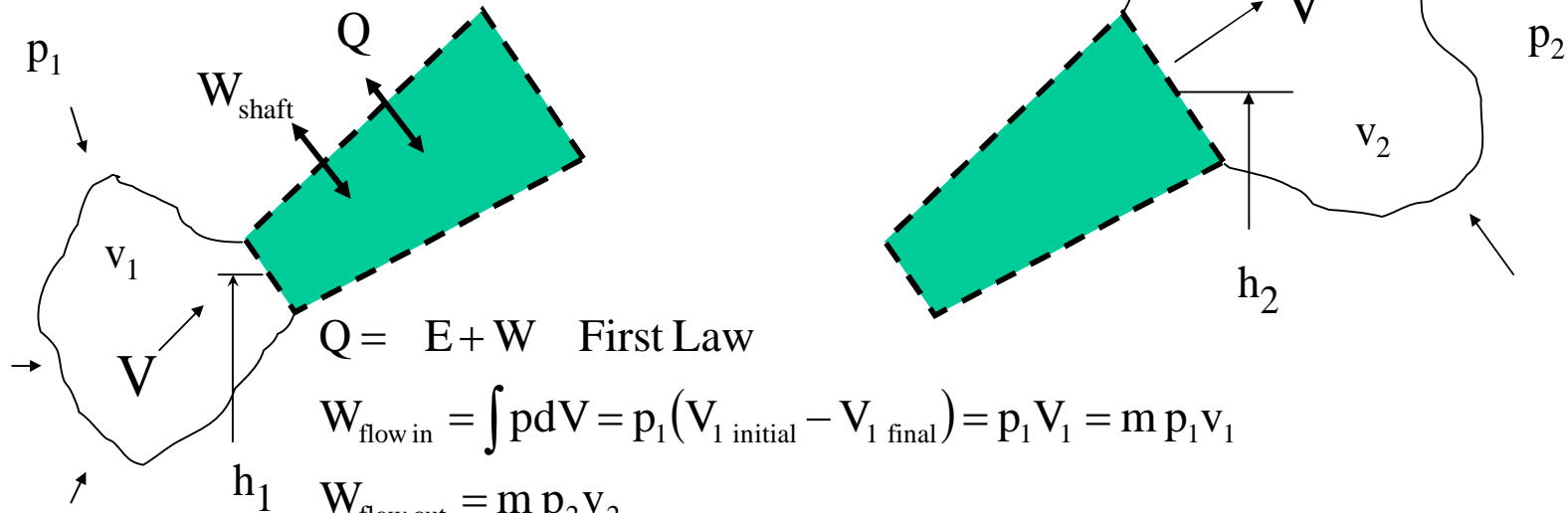


# Steady Flow Energy Equation

Open, steady flow thermodynamic system - a region in space



$$Q = E + W \quad \text{First Law}$$

$$W_{\text{flow in}} = \int p dV = p_1 (V_{1 \text{ initial}} - V_{1 \text{ final}}) = p_1 V_1 = m p_1 v_1$$

$$W_{\text{flow out}} = m p_2 v_2$$

$$W = W_{\text{shaft}} + W_{\text{flow in}} + W_{\text{flow out}} = W_{\text{shaft}} + m p_1 v_1 - m p_2 v_2$$

$$E = U(T) + \text{KE} + \text{PE} = U(T) + \frac{V^2}{2} + gh$$

$$Q = m(u_1 + p_1 v_1 + \frac{V^2}{2} + gh_1) - m(u_2 + p_2 v_2 + \frac{V^2}{2} + gh_1) + W_{\text{shaft}}$$

$$Q = m \times \Delta(u + pv + \frac{V^2}{2} + gh) + W_{\text{shaft}}$$

$$\text{KE}_{\text{ENGLISH}} = \frac{(\text{ft/sec})^2}{2 \times 32.2} = \frac{\text{ft-lb}}{\text{lb}}$$

$$\text{KE}_{\text{METRIC}} = \frac{(\text{m/sec})^2}{2 \times 1000} = \frac{\text{kJ}}{\text{kg}}$$

## Steady Flow Processes Devices

$$Q = m\Delta\left(h + \frac{V^2}{2} + gh\right) + W_{\text{shaft}} \quad \text{Steady Flow Energy Equation}$$

### Turbine, Compressor, Pump

$$\Delta\text{Velocity}, \Delta\text{Elevation}, Q = 0$$

$$W = H = m\Delta h$$

$$W = m(\mathbf{h}_{\text{in}} - \mathbf{h}_{\text{out}})$$

### Boiler, Condenser, Heat Exchanger

$$\text{Velocity} \cong 0, \quad \text{Elevation} \cong 0, \quad \text{Work} = 0$$

$$Q = H = m \Delta h$$

$$Q = m(\mathbf{h}_{\text{in}} - \mathbf{h}_{\text{out}})$$

### Diffuser, Nozzle

$$\text{Elevation} \cong 0, \quad Q = 0, \quad W = 0$$

$$\mathbf{h}_1 + \frac{V_1^2}{2} = \mathbf{h}_2 + \frac{V_2^2}{2}$$

### Valve - throttling process

$$\text{Velocity} = 0, \quad \text{Elevation} = 0, \quad Q = 0, \quad W = 0$$

$$H = 0$$

$$H_{\text{in}} = H_{\text{out}}$$

$$\mathbf{h}_{\text{in}} = \mathbf{h}_{\text{out}}$$

**What range of 850 kPa steam quality can be measured with this device?**

open thermodynamic system  
Steady Flow Energy Equation

$$Q = \left( h + \frac{V^2}{2g} + gh \right) + W_{\text{shaft}}$$

$$KE = 0, \quad PE = 0, \quad W = 0, \quad Q = 0$$

$$h_1 = h_2(T_2, P_{\text{barometer}})$$

$$h_2 @ \text{ maximum measurable quality} = h_g @ (P_{\text{barometer}} = 100. \text{ kPa})$$

$$h_2 @ \text{ maximum measurable quality} = 2505.6 \text{ kJ/kg}$$

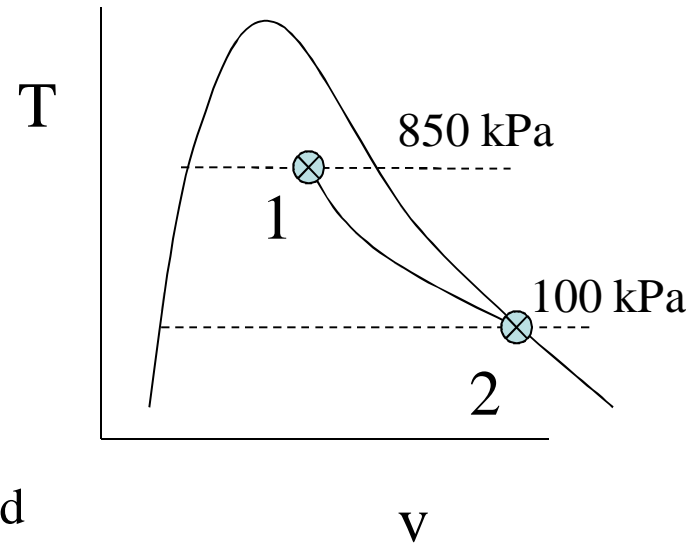
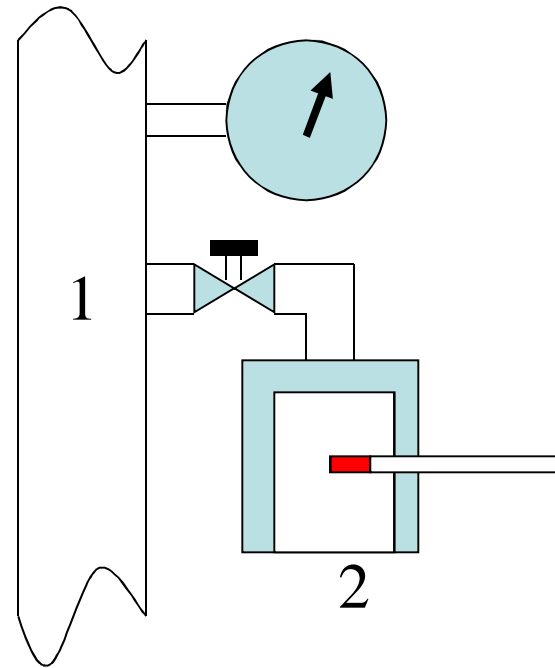
@ 850 kPa

$$h_f = 731.95 \text{ kJ/kg}$$

$$h_{fg} = 2038.8 \text{ kJ/kg}$$

$$x = \frac{h_2 - h_{1f}}{h_{1fg}} = \frac{2505.6 \text{ kJ/kg} - 731.95 \text{ kJ/kg}}{2038.8 \text{ kJ/kg}}$$

$$x = .87, \quad 87\% \text{ to } 100\% \text{ quality can be measured}$$



**500 kg/sec of 60°C water is mixed with 200 kg/sec 60°C saturated steam in a tank at a pressure of 15kPa.**

**What are the exit conditions?**

open thermodynamic system

Mass Balance  $m_c = m_a + m_b$

$m_c = 500 \text{ kg/sec} + 200 \text{ kg/sec}$

Steady Flow Energy Equation

$$Q = m\Delta\left(h + \frac{V^2}{2g} + gh\right) + W_{\text{shaft}}$$

$$Q = 0, \quad W = 0, \quad \Delta KE = 0, \quad \Delta PE = 0,$$

$m \times h = \text{constant}$

$$m_a h_a + m_b h_b = m_c h_c$$

$$h_a = h_f @ 60^\circ \text{C} = 251.18 \text{ kJ/kg}$$

$$h_b = h_v @ 60^\circ \text{C} = 2608.8 \text{ kJ/kg}$$

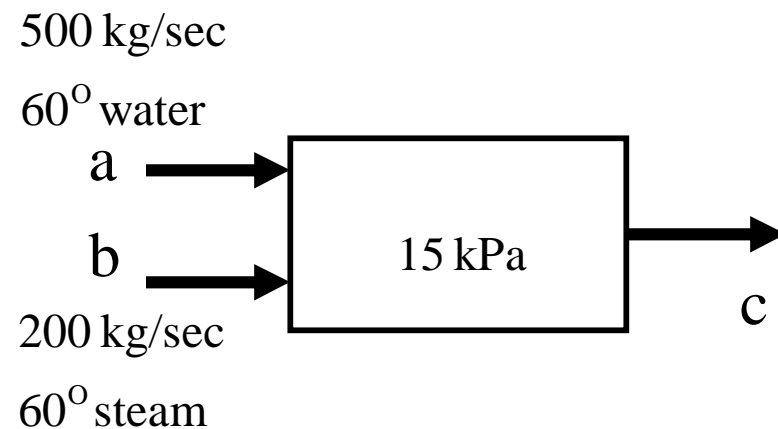
$$500 \text{ kg} \times 251.18 \text{ kJ/kg} + 200 \text{ kg} \times 2608.8 \text{ kJ/kg} = 700 \text{ kg} \times h_c$$

$$h_c = 924.79 \text{ kJ/kg}$$

$$\text{at } 15 \text{ kPa} \quad h_f = 225.94 \text{ kJ/kg}, \quad h_{fg} = 2373.3 \text{ kJ/kg}$$

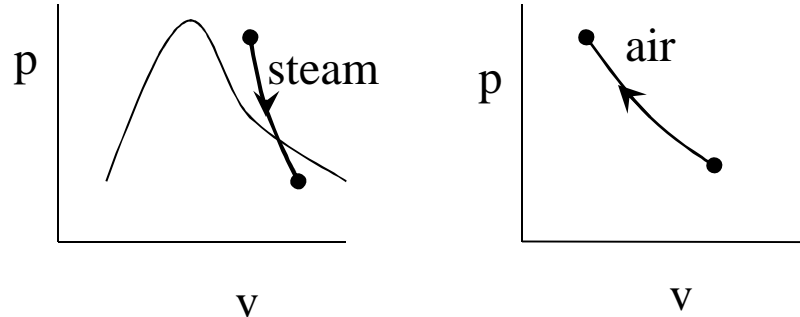
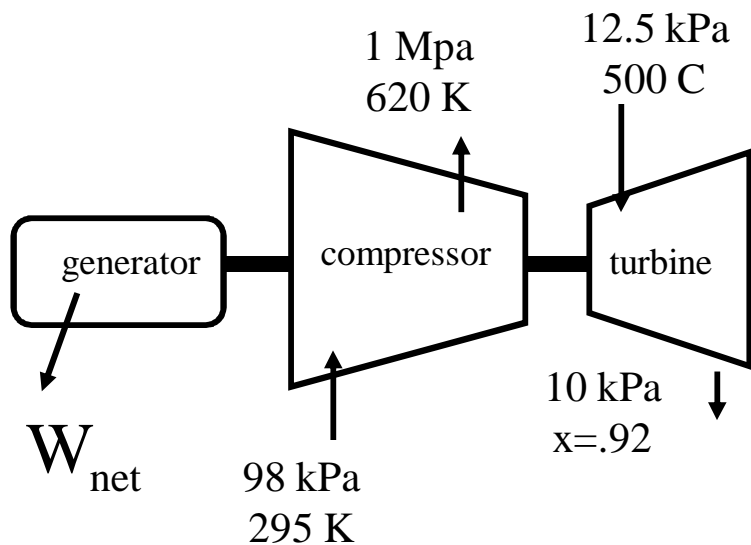
$$x = \frac{h - h_f}{h_{fg}} = \frac{924.79 - 225.94}{2372.3} = .29, \quad 29 \% \text{ quality}$$

$$T = T_{\text{saturation}} @ 15 \text{ kPa} = 53.97^\circ \text{C}$$



**An adiabatic air compressor is to be powered by a direct coupled adiabatic steam turbine that is also driving a generator. Steam enters the turbine at 12.5 MPa and 500 C at a rate of 25 kg/sec and exits at 10 kPa and a quality of .92. Air enters the compressor at 98 kpa and 295 K at a rate of 10 kg/sec and exits at 1 MPa. Determine the net power delivered to the generator by the turbine.**

An adiabatic air compressor is to be powered by a direct coupled adiabatic steam turbine that is also driving a generator. Steam enters the turbine at 12.5 MPa and 500 C at a rate of 25 kg/sec and exits at 10 kPa and a quality of .92. Air enters the compressor at 98 kPa and 295 K at a rate of 10 kg/sec and exits at 1 MPa and 620 K. Determine the net power delivered to the generator by the turbine.



$$h_{c1} = \text{airtable}@ (T = 295) = 295.17 \text{ kJ/kg Table A - 17}$$

$$h_{c2} = \text{airtable}@ (T = 620) = 628.07 \text{ kJ/kg}$$

$$h_{t1} = \text{superheat}@ (T = 500, p = 12.5 \text{ Mpa}) = 3343.6 \text{ kJ/kg}$$

$$h_{t2} = h_f @ 10\text{kPa} + xh_{fg} @ 10 \text{ kPa}$$

$$h_{t2} = 191.81 + .92 \times 2392.1 = 2392.5 \text{ kJ/kg}$$

$$W_{\text{net}} = W_{\text{turbine}} - W_{\text{compressor}} = m_t (h_{t1} - h_{t2}) - m_c (h_{c1} - h_{c2})$$

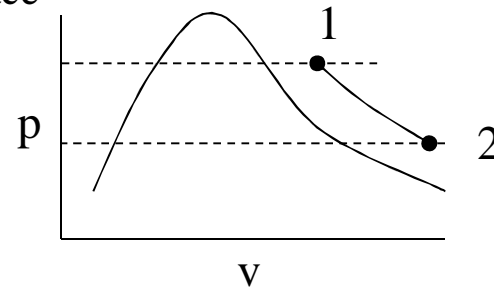
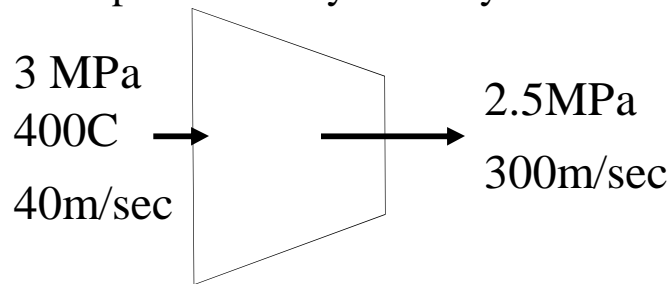
$$W_{\text{net}} = 25 \frac{\text{kg}}{\text{sec}} (3343.6 - 2392.5) - 10 \frac{\text{kg}}{\text{sec}} (628.07 - 295.17)$$

$$W_{\text{net}} = +27,106.5 \text{ kJ/sec}$$

**Steam at 3Mpa and 400 C enters an adiabatic nozzle steadily with a velocity of 40 m/sec and leaves at 2.5 MPa and 300 m/sec. Determine (a) the exit temperature and (b) the ratio of inlet to exit area.**

**Steam at 3MPa and 400 C enters an adiabatic nozzle steadily with a velocity of 40 m/sec and leaves at 2.5 MPa and 300 m/sec. Determine (a) the exit temperature and (b) the ratio of inlet to exit area.**

Open thermodynamic system - a region in space



$h_1$  &  $v_1$  = superheat @ ( $T = 400.$ ,  $P = 3.$  Mpa)

$$h_1 = 3231.7 \text{ kJ/kg}$$

$$v_1 = .09938 \text{ m}^3/\text{kg}$$

$$h_1 + \frac{V_1^2}{2} = h_2 + \frac{V_2^2}{2} \quad \text{steady flow energy equation}$$

$$h_2 = h_1 + \left( \frac{V_1^2}{2} - \frac{V_2^2}{2} \right)$$

$$h_2 = 3231.71.9 \text{ kJ/kgm} + \left( \frac{40^2}{2} - \frac{300^2}{2} \right) \frac{\text{m}^2}{\text{sec}^2} \left( \frac{1 \text{ kJ/kg}}{1000 \text{ m}^2/\text{sec}^2} \right)$$

$$h_2 = 3231.71 - 44.2 = 3187.5 \text{ kJ/kg}$$

a)  $T_2$  @ ( $h = 3187.5$ ,  $p = 2.5$ )

$$T_2 = 376.5 \text{ C,}$$

$v_2$  @ ( $h = 3187.5$ ,  $p = 2.5$ )

$$v_2 = .11626$$

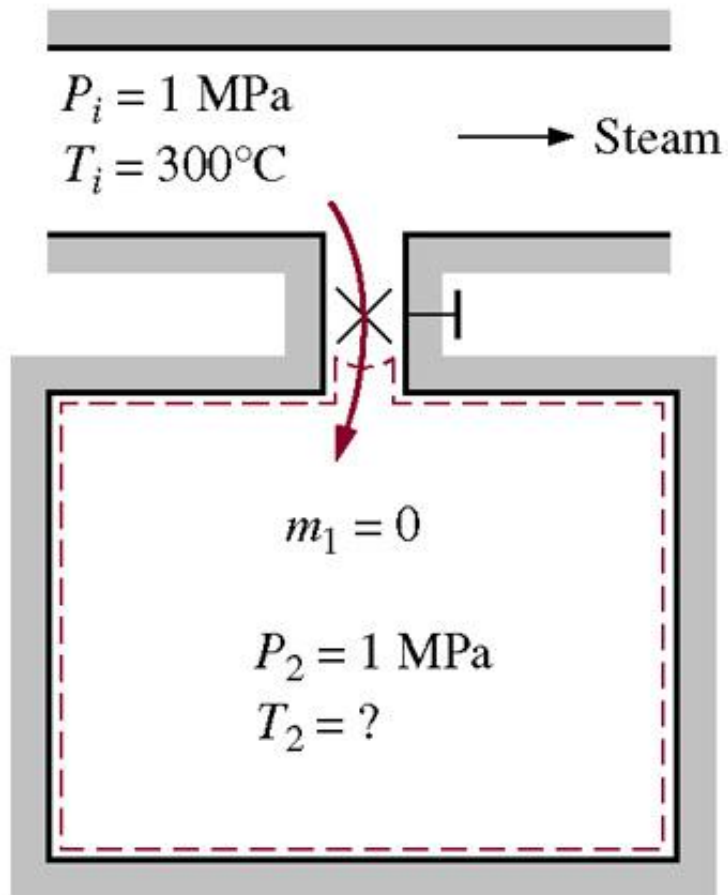
b)  $m = AV$

$$\frac{A_1 V_1}{v_1} = \frac{A_2 V_2}{v_2}$$

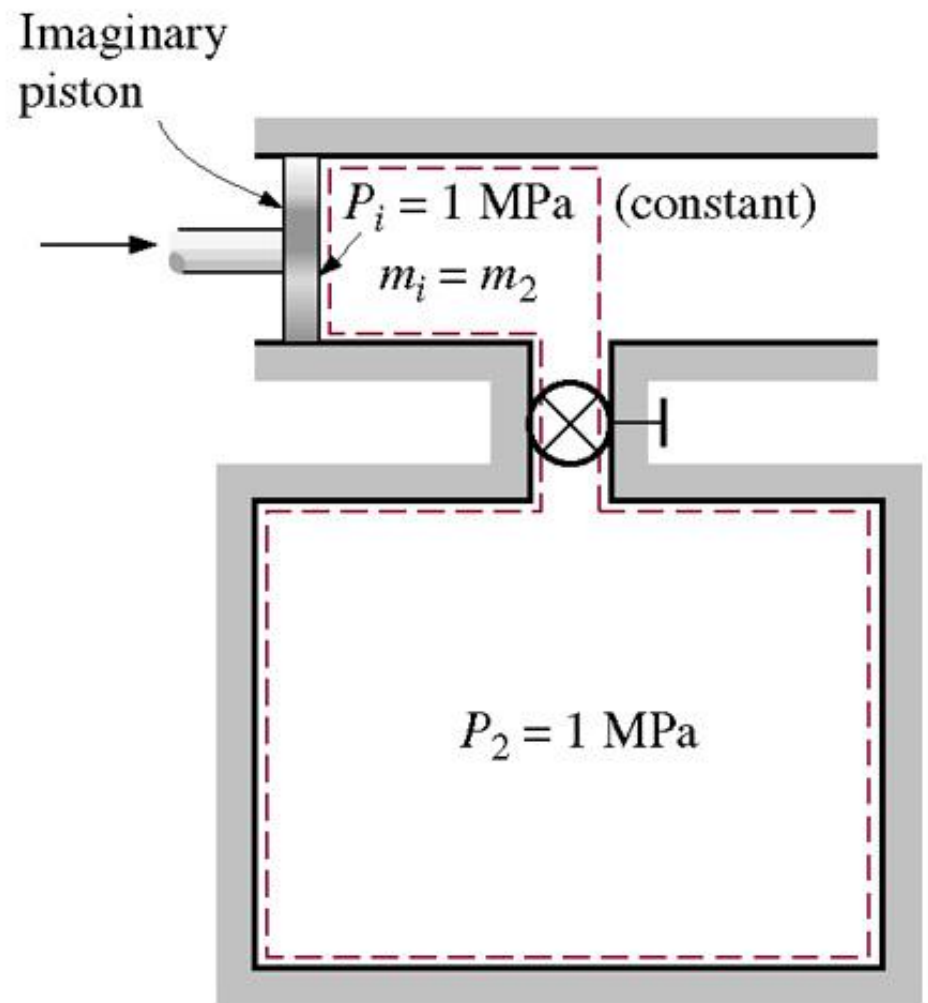
$$\frac{3 A_1 40}{.09938} = \frac{2.5 A_2 300}{.11626}$$

$$\frac{A_2}{A_1} = \frac{13.951}{74.535} = .1872$$

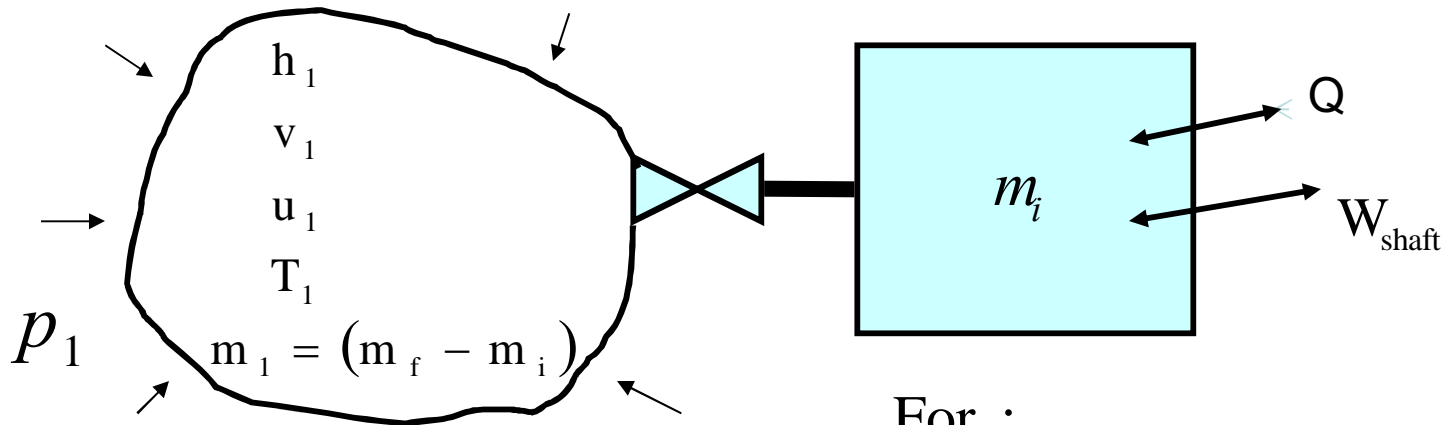




(a) Flow of steam into an evacuated tank



(b) The closed-system equivalence



system consists of initial mass in the tank plus all the mass that will flow in,  $m_f = m_i + m_1$

$$Q = E + W_{\text{flow}} + W_{\text{shaft}}$$

$$Q = E_f - E_i + W_{\text{flow}} + W_{\text{shaft}}$$

$$E_i = m_i u_i + (m_f - m_i) u_1$$

$$E_f = m_f u_f$$

$$W_{\text{flow}} = \int p dV$$

$$W_{\text{flow}} = m_1 p_1 \int dv = (m_f - m_i) p_1 (v_{\text{end}} - v_1)$$

$$W_{\text{flow}} = -(m_f - m_i) p_1 v_1$$

$$Q = m_f u_f - m_i u_i - (m_f - m_i)(u_1 + p_1 v_1) + W_{\text{shaft}}$$

For :

$$m_i = 0, \text{ a vacuum}$$

$$Q = 0$$

$$W_{\text{shaft}} = 0$$

$$u_f = h_1$$

$$c_v (T_f - T_o) = c_p (T_i - T_o)$$

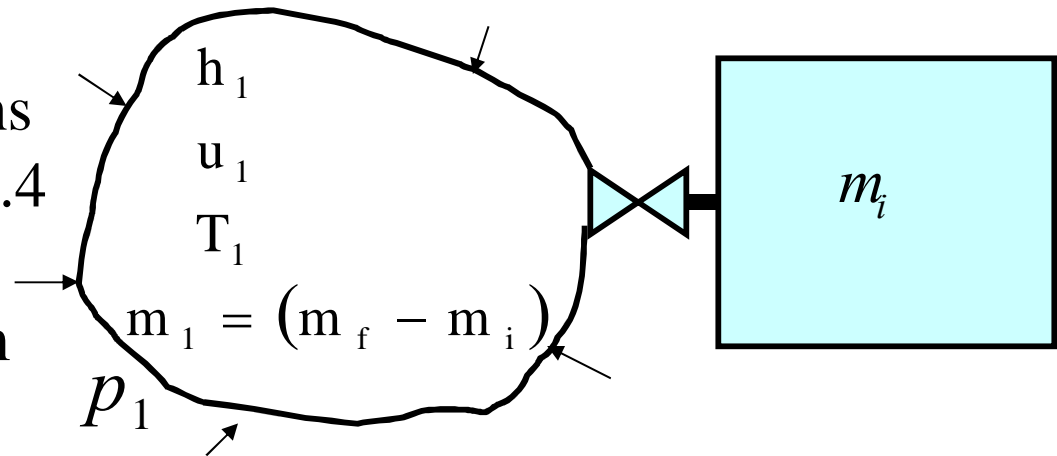
$$\frac{c_p}{c_v} = \left( \frac{T_f - T_o}{T_i - T_o} \right)$$

$$T_o \text{ is arbitrary, } T_o = 0$$

$$T_f = k T_1$$

$$Q = m_f u_f - m_i u_i - (m_f - m_i)(u_1 + p_1 v_1) + W_{\text{shaft}}$$

A 200 cubic ft tank contains 2. lbm carbon dioxide and .4 lbm helium at an initial temperature of 70 F. 3 lbm of air at 14.7 and 70 F are admitted to the tank.



What is the final temperature of the tank?

$$Q = m_f u_f - m_i u_i - (m_f - m_i)(h_i)$$

$$m_f u_f = (3 \times .174 + 2 \times .1565 + .4 \times .745) T_f = 1.125 T_f$$

$$m_i u_i = (2 \times .1565 + .4 \times .745) \times (460 + 70) = 323.83$$

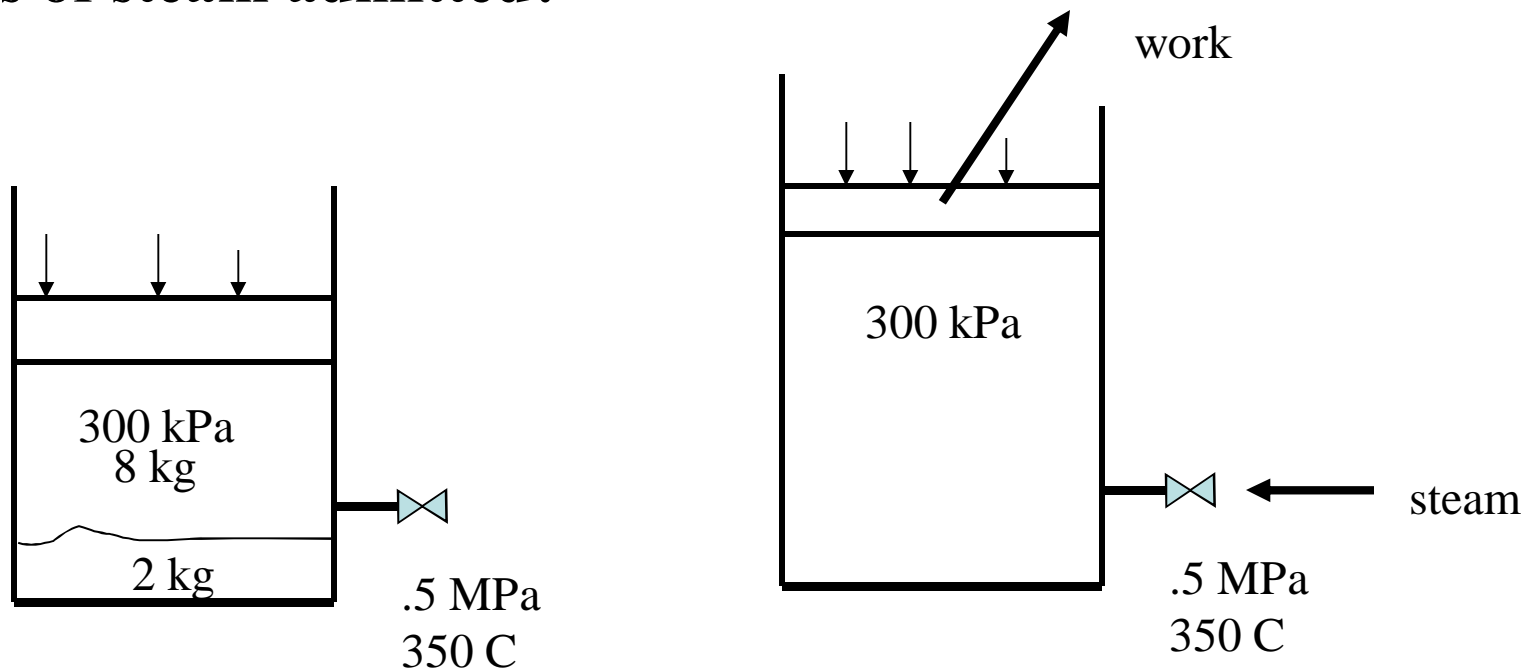
$$(m_i - m_f) \times h_1 = 3 \times .24 \times (460 + 70) = 381.6$$

$$Q = 1.125 T_f - 323.83 - 381.6 = 0$$

$$T_f = 627^\circ \text{R}$$

$$T_f = 167^\circ \text{F}$$

**There initially are 2 kg of liquid water and 8 kg of vapor in an insulated vertical piston cylinder device. A constant pressure of 300 kPa is maintained by the piston weight. Steam at .5 MPa and 350 C are added until the contents of the cylinder are all vapor. What is the final temperature in the cylinder and the mass of steam admitted?**



the system is the mass finally in the cylinder,  $m_f$

$$E_i = m_i u_i + (m_f - m_i) u_o$$

$$E_f = m_f u_f$$

$$W_{\text{flow}} = \int p dv = p_o (V_{oi} - V_{of})$$

$$W_{\text{flow}} = (m_f - m_i) p_o v_o$$

$$W_{\text{displacement}} = \int p dv = p_f (V_f - V_i)$$

$$W_{\text{displacement}} = p_f V_f - p_i V_i$$

$$W_{\text{displacement}} = m_f p_f v_f - m_i p_i v_i$$

$$0 = E_f - E_i - W_{\text{flow}} + W_{\text{displacement}} \quad \text{First Law}$$

$$0 = m_f u_f - m_i u_i - (m_f - m_i) u_o - (m_f - m_i) p_o v_o + m_f p_f v_f - m_i p_i v_i$$

$$0 = (m_f u_f + m_f p_f v_f) - (m_i u_i + m_i p_i v_i) - (m_f - m_i) u_o - (m_f - m_i) p_o v_o$$

$$0 = m_f h_f - m_i h_i - (m_f - m_i) h_o$$

$$0 = m_f h_f - m_i h_i - m_f h_o + m_i h_o$$

$$0 = m_f (h_f - h_o) + m_i (h_o - h_i)$$

$$m_f = m_i \frac{(h_o - h_i)}{(h_o - h_f)}$$

$$m_f = 10 \text{ kg} \frac{(3168.1 \text{ kJ/kg} - 2292.23 \text{ kJ/kg})}{(3168.17 \text{ kJ/kg} - 2724.9 \text{ kJ/kg})} = 19.76 \text{ kg}$$

$$m_f - m_i = 19.76 \text{ kg} - 10 \text{ kg} = 9.76 \text{ kg}$$

@ 300 kPa

$$h_{\text{final}} = h_g = 2724.9 \text{ kJ/kg}$$

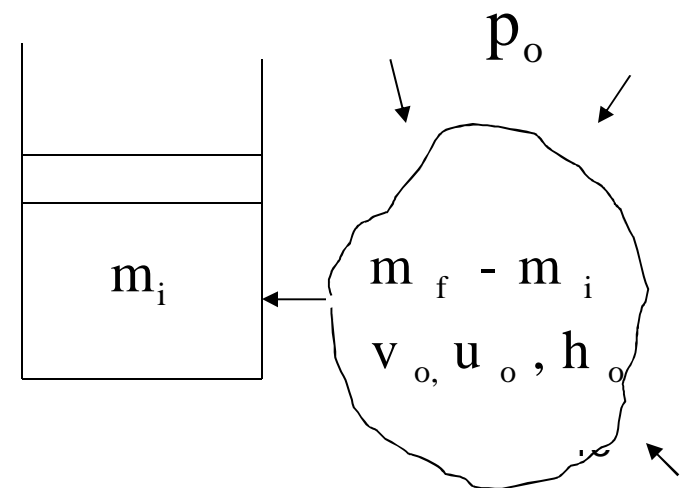
$$h_i = h_f + x \times h_{fg}$$

$$h_i = 561.43 + .8 \times 2163.5$$

$$h_i = 2292.23 \text{ kJ/kg}$$

@ .5 MPa, 350°C

$$h_o = 3168.1 \text{ kJ/kg}$$



## First Law

Energy defined , Energy conserved

$$E_{in} - E_{out} = E$$

E is all forms, Q, W, PE, KE, U

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) + (E_{mass\ in} - E_{mass\ out}) = U_2 - U_1$$

### CLOSED SYSTEM a contained quantity of mass

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) + (\cancel{E_{mass\ in}} - \cancel{E_{mass\ out}}) = U_2 - U_1$$

0

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) = U_2 - U_1$$

$$Q = U_2 - U_1 + W$$

$$Q = E + W$$

### OPEN SYSTEM a region in space

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) + (\cancel{E_{mass\ in}} - \cancel{E_{mass\ out}}) = U_2 - U_1$$

0

$$W = W_{shaft} + W_{flow}$$

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) = (E_{mass\ out} - E_{mass\ in})$$

$$\text{for } W_{net} = 0, \quad Q = H_2 - H_1 = m(h_2 - h_1)$$

$$\text{for } Q_{net} = 0, \quad W = H_2 - H_1 = m(h_2 - h_1)$$

## UNSTEADY SYSTEM

quantity of mass,  $m_1$  or  $m_2$

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) + (E_{mass\ in} - E_{mass\ out}) = U_2 - U_1$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (W_{flow\ in} - W_{flow\ out}) = U_2 - U_1$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (p_o V_o)_{in} - (p_o V_o)_{out} = U_2 - U_1$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (m_2 - m_1)(p_o v_o)_{in} - (m_2 - m_1)(p_o v_o)_{out} =$$

$$m_2 u_2 - m_1 u_1 + (m_2 - m_1)u_{out} - (m_2 - m_1)u_{in}$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (m_2 - m_1)h_{in} - (m_2 - m_1)h_{out} = m_2 u_2 - m_1 u_1$$

with  $W_{out}$ ,  $Q_{in}$ , +

$$Q - W + (m_2 - m_1)h = m_2 u_2 - m_1 u_1$$

## UNSTEADY SYSTEM

region in space

$$(Q_{in} - Q_{out}) + (W_{in} - W_{out}) + (E_{mass\ in} - E_{mass\ out}) = U_2 - U_1$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (E_{mass\ in} - E_{mass\ out}) = U_2 - U_1$$

$$(Q_{in} - Q_{out}) + (W_{b\ in} - W_{b\ out}) + (m_2 - m_1)h_{in} - (m_2 - m_1)h_{out} = m_2 u_2 - m_1 u_1$$