

mae 422

Problem Set 3 (PS3) Due Tuesday February 7

1. Derive in detail for 1 –D flow with heat transfer, the Rayleigh Flow equations, 3.78 and 3.81.
  2. At a point in an isentropic flow,  $T=280$  K,  $P=100$  kPa,  $v=100$  m/sec. What are the stagnation properties of this flow ? To what value would the pressure have to be reduced to achieve sonic flow in the duct ?
  3. What friction factor is required to accelerate a flow from 300 K, 100 kPa, 6.94 m/sec to sonic in a constant area duct with a diameter of .5 m and a length of 6000 m ?
- 3.9 and 3.10 in the Anderson Text.

## PS 3.1

energy equation  $q + h_1 + \frac{u_1^2}{2} = h_2 + \frac{u_2^2}{2}$

momentum equation  $p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2$

sonic velocity  $a^2 = \gamma RT$

ideal gas  $p = \rho RT$

since by definition,  $u^2 = a^2 M^2$ ,

and for an ideal gas,  $a^2 = \gamma RT = \frac{\gamma p}{\rho}$

substituting into the momentum equation,

$$p_2 - p_1 = \rho_1 u_1^2 - \rho_2 u_2^2 = \rho_1 a_1^2 M_1^2 - \rho_2 a_2^2 M_2^2$$

$$p_2 - p_1 = \rho_1 \frac{\gamma p_1}{\rho_1} M_1^2 - \rho_2 \frac{\gamma p_2}{\rho_2} M_2^2$$

dividing by  $p_1$ ,

$$\frac{p_2}{p_1} - 1 = \rho_1 \frac{\gamma p_1}{\rho_1 p_1} M_1^2 - \rho_2 \frac{\gamma p_2}{\rho_2 p_1} M_2^2$$

$$\frac{p_2}{p_1} (1 + \gamma M_2^2) = 1 + \gamma M_1^2$$

$$\frac{p_2}{p_1} = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2} \quad (3.78)$$

continuity  $\rho_1 u_1 = \rho_2 u_2$

for an ideal gas,  $\rho = \frac{p}{RT}$

substituting into continuity,

$$\frac{p_1}{RT_1} u_1 = \frac{p_2}{RT_2} u_2$$

$$\frac{T_2}{T_1} = \frac{p_2 u_2}{p_1 u_1}$$

from definition of Mach Number

$$\frac{u_2}{u_1} = \frac{M_2 a_2}{M_1 a_1} = \frac{M_2}{M_1} \left( \frac{\gamma RT_2}{\gamma RT_1} \right)^{\frac{1}{2}}$$

substituting,

$$\frac{T_2}{T_1} = \frac{p_2}{p_1} \frac{M_2}{M_1} \left( \frac{\gamma RT_2}{\gamma RT_1} \right)^{\frac{1}{2}}$$

$$\left( \frac{T_2}{T_1} \right)^{\frac{1}{2}} = \frac{p_2}{p_1} \frac{M_2}{M_1}$$

$$\frac{T_2}{T_1} = \left( \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2} \right)^2 \left( \frac{M_2}{M_1} \right)^2 \quad (3.81)$$

## PS 3.2

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P= 100 kPa	1	2
T= 280 K	○	○ M=1
V=200 m/sec		

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$$a_1 = \sqrt{\gamma RT} = \sqrt{1.4 \times .287 \times 1000 \times 280} = 335.4 \text{ m/sec}$$

$$M_1 = \frac{100}{335.4} = .3$$

$$@ M = .6, \frac{p_0}{p_1} = \left(1 + \frac{\gamma - 1}{2} M^2\right)^{\frac{\gamma}{\gamma - 1}} = 1.276 \text{ or Table A.1}$$

$$p_0 = 1.276 \times 100 = 127.6 \text{ kPa}$$

$$\frac{T_0}{T} = 1.072$$

$$T_0 = 1.072 \times 280 = 300.16 \text{ K}$$

$$@ M = 1, \frac{p_0}{p_2} = 1.893$$

$$\left(\frac{p_0}{p_2}\right) = \left(\frac{p_0}{p_1}\right) \frac{p_1}{p_2}$$

$$1.893 = 1.276 \frac{p_1}{p_2}$$

$$p_2 = \frac{1.276 p_1}{1.893} = .674 \times 100 = 67.4 \text{ kPa}$$

### PS 3.3

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300 K	1	2
100 kPa	○	○
6.94 m/sec		M=1

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$$a_1 = \sqrt{\gamma RT_1} = \sqrt{1.4 \times .287 \times 1000 \times 300} = 347.2$$

$$M_1 = \frac{6.94}{347.2} = .02$$

$$@ M_1 = .02, \quad \frac{4fL^*}{D} = 1778 \quad (3.107) \text{ or Table A.4}$$

$$f = \frac{1778 \times .5}{4 \times 6000} = .037$$

$$q = \frac{3.9 \times 4.5 \times 10^8 \text{ ft lbf}}{\text{slug}} \frac{1 \text{ slug}}{32.2 \text{ lb fuel}} \frac{1 \text{ Btu}}{778 \text{ ft lbf}} \frac{.06 \text{ lbm fuel}}{\text{lbm air}} \frac{1 \text{ lb air}}{1.06 \text{ lb products}}$$

$$q = 1016.8 \frac{\text{Btu}}{\text{lb products}}$$

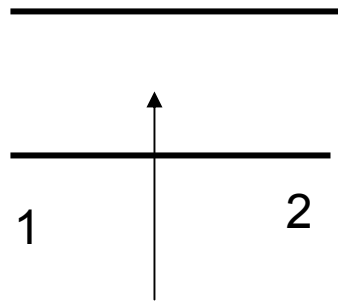
$$q = c_p (T_{O2} - T_{O1})$$

$$\frac{q}{c_p T_{O1}} = \frac{T_{O2}}{T_{O1}} - 1$$

$$1 + \frac{q}{c_p T_1 \frac{T_{O1}}{T_1}} = \frac{T_{O2}}{T_{O1}}$$

$$1 + \frac{q}{c_p T_1 \frac{T_{O1}}{T_1}} = \frac{T_{O2}}{T_O^*} \frac{T_O^*}{T_{O1}} \quad (a)$$

10 atm  
1000 R  
M=.2



$$q = \frac{4.5 \times 10^8 \text{ ft lbf}}{\text{slug}}$$

substituting into (a),

$$1 + \frac{q}{c_p T_1 \frac{T_{O1}}{T_1}} = \frac{T_{O2}}{T_O^*} \frac{T_O^*}{T_{O1}}$$

$$1 + \frac{1016.8}{.24 \times 1000 \times 1.008} = \frac{T_{O2}}{T_O^*} \frac{1}{.1736}$$

$$\frac{T_{O2}}{T_O^*} = .903$$

Table A.3 @  $\frac{T_{O2}}{T_O^*} = .903$ ,

$$M = .96, \frac{p_2}{p^*} = 1.433, \frac{T_2}{T^*} = .9895$$

$$p_2 = \frac{p_2}{p^*} \frac{p^*}{p_1} p_1 = 1.433 \frac{1}{2.273} \times 10 = 6.30 \text{ atm}$$

$$T_2 = \frac{T_2}{T^*} \frac{T^*}{T_1} \times T_1 = .9895 \frac{1}{.2066} \times 1000 = 4789 \text{ R}$$

Table A.1 @ M = .2

$$\frac{T_{O1}}{T_1} = 1.008$$

Table A.3 @ M = .2

$$\frac{T_{O1}}{T_O^*} = .1736, \frac{p_1}{p^*} = 2.273, \frac{T_1}{T_O^*} = 2.066$$

### 3.10

Table A.3 @  $M_2 = 1, \frac{T_{O2}}{T_O^*} = 1$

From 3.9,

$$1 + \frac{q}{c_p T_1 \frac{T_{O1}}{T_1}} = \frac{T_{O2}}{T_O^*} \frac{T_O^*}{T_{O1}} \quad (\text{a})$$

$$1 + \frac{q}{.24 \times 1000 \times 1.008} = 1 \times \frac{1}{.1736}$$

$$q = 1151.6 \text{ Btu/lb products}$$

$$q = \frac{4.5 \times 10^8 \times \text{AF}}{(1 + \text{AF}) \times 778 \times 32.2} = 1151.5 \text{ Btu/lb products}$$

$$\text{AF} = .0685$$