

Problem Set 12 (PS12) due
Monday April. 23
10.10 10.13 10.32 10.34

10.10

$$\frac{u}{U_e} = \sin \frac{\pi y}{2\delta} \quad (y \leq \delta)$$

Continuity equation :

$$-U_e \delta w + \int_0^\delta u w dy + \int_0^{L^-} v w dx = 0$$

x - momentum equation :

(-F = force by plate on fluid)

$$-F = -\rho U_e^2 \delta w + \int_0^\delta \rho u^2 w dy + \int_0^L \rho U_e \bar{v} w dx$$

From the two equations, we get:

$$\therefore -F = -\rho U_e^2 \delta w + \rho U_e^2 \delta w + \int_0^\delta (\rho u^2 - \rho U_e u) w dy$$

$$\begin{aligned} \therefore \frac{F}{\rho U_e^2 \delta w} &= \int_0^\delta \left(\frac{u}{U_e} - \left(\frac{u}{U_e} \right)^2 \right) dy \\ &= \int_0^\delta \left(\sin \frac{\pi y}{2\delta} - \sin^2 \frac{\pi y}{2\delta} \right) dy = \frac{4 - \pi}{2\pi} \end{aligned}$$

10.13

$$(a) R_{e_x} = \frac{xU_e}{\nu}$$

$$\text{for } x=1\text{m}, U_e = 20\text{m/s}, \nu = 1.56 \times 10^{-5} \text{ m}^2/\text{s}$$

$$R_{e_x} = 1.28 \times 10^6$$

Since $R_{e_x} > 10^5$, we should expect flow near trailing edge to be turbulent.

(b) Using a $\frac{1}{7}$ power law, assuming that the boundary

layer is turbulent from the leading edge then at $x=1\text{m}$:

$$\frac{\delta}{x} = \frac{0.37}{R_{e_x}^{0.2}} = \frac{0.37}{(1.28 \times 10^6)^{0.2}} = 0.022$$

$$\therefore \delta = 22 \text{ mm (max value)}$$

$$(c) \text{From equation 10.21, } C_F = \frac{0.074}{R_L^{0.2}} = \frac{0.074}{(1.28 \times 10^6)^{0.2}}$$

(assuming boundary layer is turbulent from leading edge)

$$\therefore C_F = 0.00444$$

$$(d) C_F = \frac{F_V}{\frac{1}{2} \rho U_e^2 L w}$$

$$\therefore 2F_V = \rho U_e^2 L w \times C_F = \text{total drag}$$

$$\therefore \text{total drag on plate} = 1.184 \times (20)^2 \times 1 \times 0.5 \times 0.00444 \text{ N} \\ = 1.05 \text{ N}$$

10.32

$$R_e = \frac{DU_\infty}{\nu} = 25100$$

If we model the flow on the flow over an isolated cylinder of infinite length,

$$C_D = 1.5$$

$$= \frac{F}{\frac{1}{2} \rho U_\infty^2 DL}$$

$$\therefore F = \frac{1}{2} \rho U_\infty^2 DL \times C_D$$

$$= \frac{1}{2} \times 2.469 \times 10^{-3} \times \left(60 \times \frac{22}{15}\right)^2 \times \frac{0.5}{12} \times 120 \times 1.5 \text{ lbf}$$

$$= 72 \text{ lbf}$$

10.34

$$(a) C_D = \frac{F}{\frac{1}{2} \rho U_\infty^2 A} \quad (A = \text{frontal area})$$

$$\therefore F = \frac{1}{2} \rho U_\infty^2 A \times C_D$$

$$= \frac{1}{2} \times \frac{2.373}{1000} \times (75 \times \frac{22}{15})^2 \times 24 \times 0.4 \text{ lbf}$$

$$= 138 \text{ lbf}$$

$$(b) \text{From definition of } C_D : U_\infty^2 = \frac{F}{\frac{1}{2} \rho A C_D}$$

$$\text{That is: } U_\infty^3 = \frac{F \times U_\infty}{\frac{1}{2} \rho A C_D} = \frac{P}{\frac{1}{2} \rho A C_D}$$

$$\text{where } P = F \times U_\infty = \text{available power} = 0.8 \times 120 \text{ hp} \\ = 0.8 \times 120 \times 550 \text{ ft} \cdot \text{lbf/s}$$

If only source of drag was aerodynamic:

$$U_\infty^3 = \frac{P}{\frac{1}{2} \rho A C_D} = \frac{0.8 \times 120 \times 550}{\frac{1}{2} \times \frac{2.737}{1000} \times 30 \times 0.6} \left(\frac{\text{ft}}{\text{s}}\right)^3$$

$$\therefore (U_\infty)_{\max} = 135 \frac{\text{ft}}{\text{s}} = 92 \text{ mph}$$

U_∞ is a relative velocity, and if there is a 30mph headwind

$$(U_\infty)_{\max} = 92 - 30 \text{ mph} = 62 \text{ mph}$$