

Differential Equations
Chapter 6.1-6.3, 1.4, 1.5

MATH REVIEW

Gauss's Theorem - Divergence Theorem

transforms a surface integral into a volume integral

$$\oiint_A (\vec{n} \bullet \vec{V}) dA = \iiint_{\text{vol}} (\nabla \cdot \vec{V}) d \text{ vol} \quad \text{where: } (\vec{V}) \text{ is a vector}$$

$$\oiint_A (a) dA = \iiint_{\text{vol}} (\nabla a) d \text{ vol} \quad \text{where: } (a) \text{ is a scalar}$$

Gradient $\nabla = \frac{\partial(\)}{\partial x} \vec{i} + \frac{\partial(\)}{\partial y} \vec{j} + \frac{\partial(\)}{\partial z} \vec{k}$

∇ of a vector is a scalar

∇ of a scalar is a vector

CONTINUITY EQUATION CONSERVATIVE INTEGRAL FORM

Gauss's Theorem transforms a surface integral into a volume integral

$$\oiint_A \vec{n} \bullet \vec{V} dA = \iiint_{\text{vol}} \nabla \cdot \vec{V} d \text{ vol} \quad \text{where, } \nabla = \frac{\partial}{\partial x} + \frac{\partial}{\partial y} + \frac{\partial}{\partial z}$$

Δ (control volume mass) = net mass outflow

$$\frac{\partial}{\partial t} \iiint_{\text{vol}} \rho d \text{ vol} = - \oiint_A \left(\rho \vec{n} \bullet \vec{V} \right) dA$$

by Smits convention mass inflow is - .

applying Gauss's Theorem to the net mass outflow term,

CONTINUITY EQUATION CONSERVATIVE INTEGRAL FORM

$$\iiint_{\text{vol}} \frac{\partial}{\partial t} \rho \, d \text{ vol} = - \iiint_{\text{vol}} \nabla(\rho \vec{V}) \, d \text{ vol}$$

differentiating,

$$\frac{\partial \rho}{\partial t} + \nabla(\rho \vec{V}) = 0 \quad (6.7)$$

Unsteady, 3 - D, any fluid, variable density

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} = 0 \quad (6.6)$$

substituting, $\frac{\partial(\rho u)}{\partial x} = u \frac{\partial \rho}{\partial x} + \rho \frac{\partial u}{\partial x}$ in x, y and z

$$\frac{\partial \rho}{\partial t} + \left(u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} \right) + \left(\rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + \rho \frac{\partial w}{\partial z} \right) = 0 \quad)$$

Steady, incompressible flow

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

MONENTUM EQUATION CONSERVATIVE INTEGRAL FORM

$$\oint_A (\rho \vec{n} \cdot \vec{V}) \vec{V} dA + \iiint_{\text{vol}} \frac{\partial(\rho \vec{V})}{\partial t} d \text{vol} = \iiint_{\text{vol}} \rho f d \text{vol} - \oint_S p dS + \oint_S \tau dS$$

using Gauss' s Therom

$$\oint_A \vec{V} dA = \iiint_{\text{vol}} (\nabla \cdot \vec{V}) d \text{vol} \quad \text{and} \quad \oint_S (a) dS = \iiint_{\text{vol}} (\nabla a) d \text{vol}$$

to convert the three surface integrals to volume inteagrals

$$\iiint_{\text{vol}} \nabla(\rho \vec{V}) \cdot \vec{V} d \text{vol} + \iiint_{\text{vol}} \frac{\partial(\rho \vec{V})}{\partial t} d \text{vol} = \iiint_{\text{vol}} \rho f d \text{vol} - \iiint_{\text{vol}} \nabla p d \text{vol} + \iiint_{\text{vol}} \nabla \tau d \text{vol}$$

differentiating

$$\frac{\partial(\rho \vec{V})}{\partial t} = -\nabla p - \nabla(\rho \vec{V}) \cdot \vec{V} - \nabla \tau + \rho f$$

MOMENTUM EQUATIONS

unsteady, 3D, any fluid, variable density

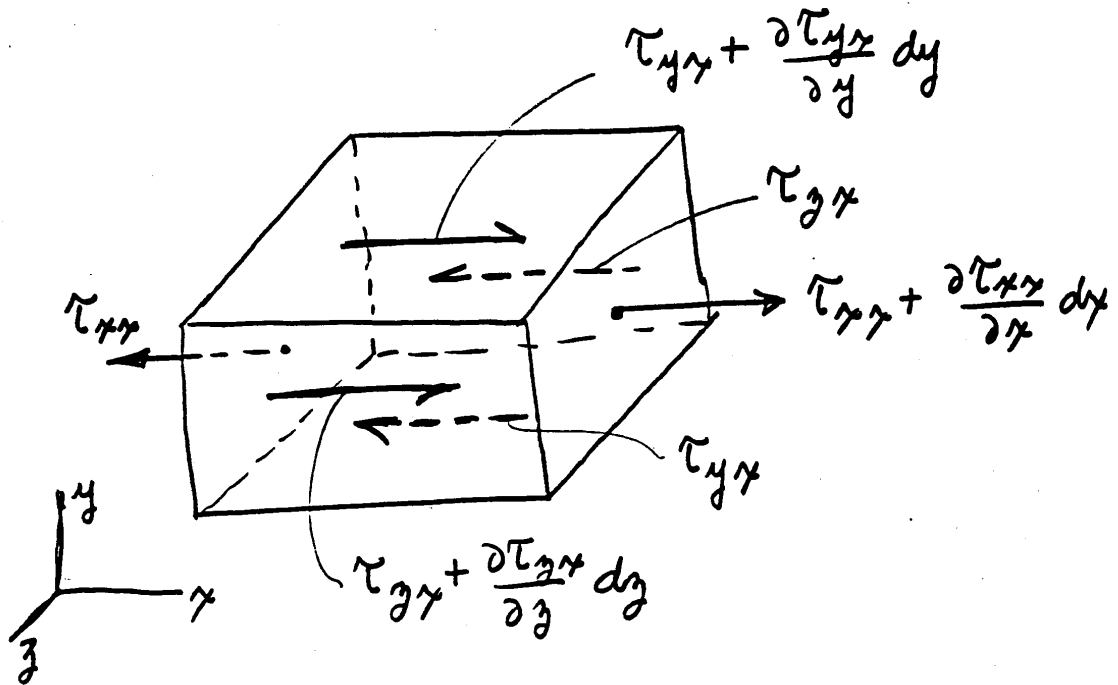
$$\frac{\partial(\rho \vec{V})}{\partial t} = -\nabla p - \nabla(\rho \vec{V})\vec{V} - \nabla\tau + \rho \mathbf{f}$$

$$\frac{\partial}{\partial t} \rho u = -\frac{\partial p}{\partial x} - \left(\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial y} + \rho w \frac{\partial u}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{yx} + \frac{\partial}{\partial z} \tau_{zx} \right) + \rho f_x$$

$$\frac{\partial}{\partial t} \rho v = -\frac{\partial p}{\partial y} - \left(\rho u \frac{\partial v}{\partial x} + \rho v \frac{\partial v}{\partial y} + \rho w \frac{\partial v}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xy} + \frac{\partial}{\partial y} \tau_{yy} + \frac{\partial}{\partial z} \tau_{zy} \right) + \rho f_y$$

$$\frac{\partial}{\partial t} \rho w = -\frac{\partial p}{\partial z} - \left(\rho u \frac{\partial w}{\partial x} + \rho v \frac{\partial w}{\partial y} + \rho w \frac{\partial w}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xz} + \frac{\partial}{\partial y} \tau_{yz} + \frac{\partial}{\partial z} \tau_{zz} \right) + \rho f_z$$

NEWTON'S LAW FOR GENERAL FLOW



$$\begin{aligned}
 dF_x &= \left(\tau_{xx} + \frac{\partial \tau_{xx}}{\partial x} dx \right) dy dz - \tau_{xx} dy dz \\
 &+ \left(\tau_{yx} + \frac{\partial \tau_{yx}}{\partial y} dy \right) dx dz - \tau_{yx} dx dz \\
 &+ \left(\tau_{zx} + \frac{\partial \tau_{zx}}{\partial z} dz \right) dx dy - \tau_{zx} dx dy \\
 &= \left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) dx dy dz
 \end{aligned}$$

$$\rho \frac{DN_x}{Dt} = \rho B_x + \frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z}$$

$$\tau_{ij} = \begin{pmatrix} -p + \tau'_{xx} & \tau'_{xy} & \tau'_{xz} \\ \tau_{yx} & -p + \tau'_{yy} & \tau'_{yz} \\ \tau'_{zx} & \tau'_{zy} & -p + \tau'_{zz} \end{pmatrix}$$

τ'_{ij} DUE TO FRICTION

$$e \frac{DV_x}{Dt} = -\frac{\partial p}{\partial x} + e B_x + \frac{\partial \tau'_{xx}}{\partial x} + \frac{\partial \tau'_{xy}}{\partial y} + \frac{\partial \tau'_{xz}}{\partial z}$$

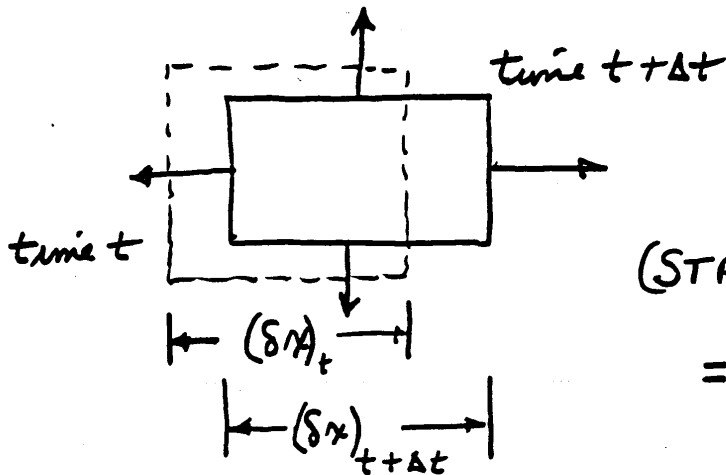
$$e \frac{DV_y}{Dt} = -\frac{\partial p}{\partial y} + e B_y + \frac{\partial \tau'_{xy}}{\partial x} + \frac{\partial \tau'_{yy}}{\partial y} + \frac{\partial \tau'_{yz}}{\partial z}$$

$$e \frac{DV_z}{Dt} = -\frac{\partial p}{\partial z} + e B_z + \frac{\partial \tau'_{xz}}{\partial x} + \frac{\partial \tau'_{yz}}{\partial y} + \frac{\partial \tau'_{zz}}{\partial z}$$

NEED TO RELATE τ'_{ij} TO THE STRAIN FIELD

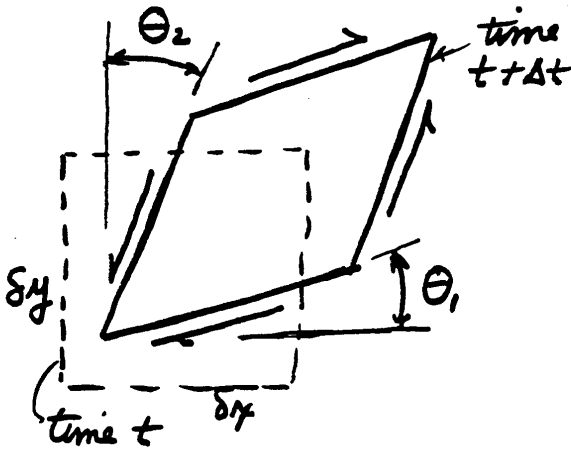
STRESS + STRAIN

NORMAL STRESS \rightarrow ELONGATION



$$\begin{aligned} (\text{STRAIN})_x &= \epsilon_{xx} \\ &= \frac{(\delta x)_{t + \Delta t} - (\delta x)_t}{(\delta x)_t} \end{aligned}$$

SHEAR STRESS \rightarrow CHANGE IN ANGLE

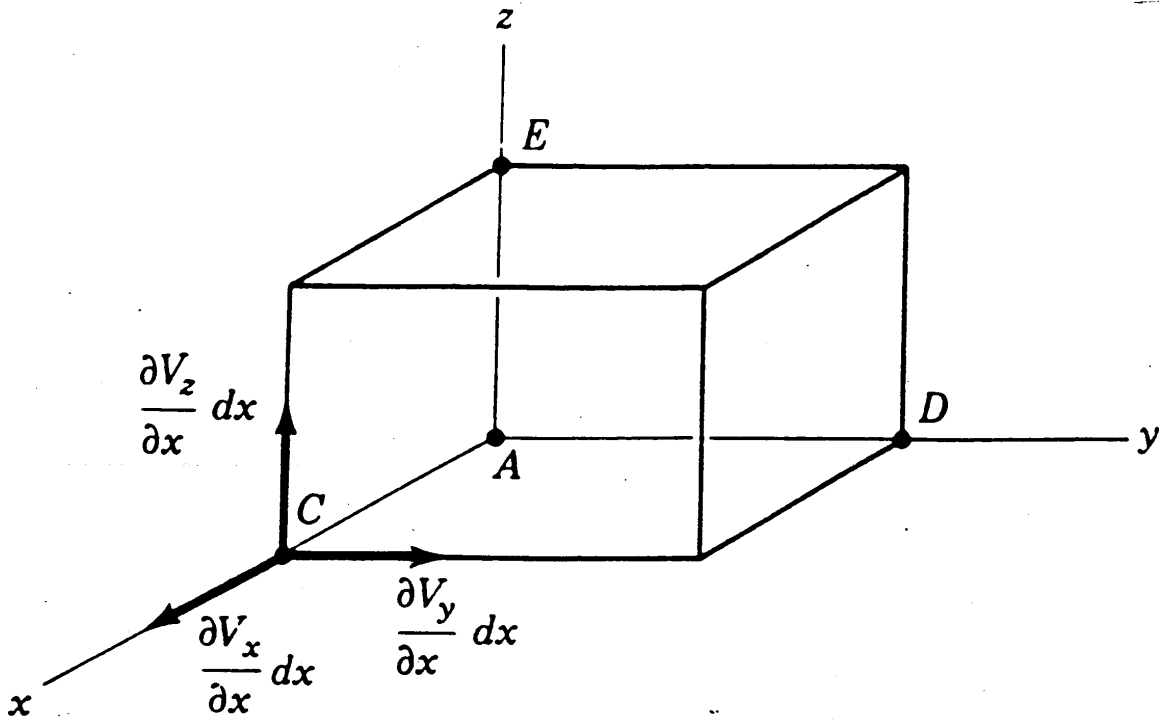


$$\begin{aligned} (\text{STRAIN})_{xy} &= \epsilon_{xy} \\ &= \theta_1 + \theta_2 \end{aligned}$$

$$\tau_{xy} \propto \epsilon_{xy}$$

$$(\text{Rotation})_z = \frac{1}{2}(\theta_1 - \theta_2)$$

STRAIN + ROTATION



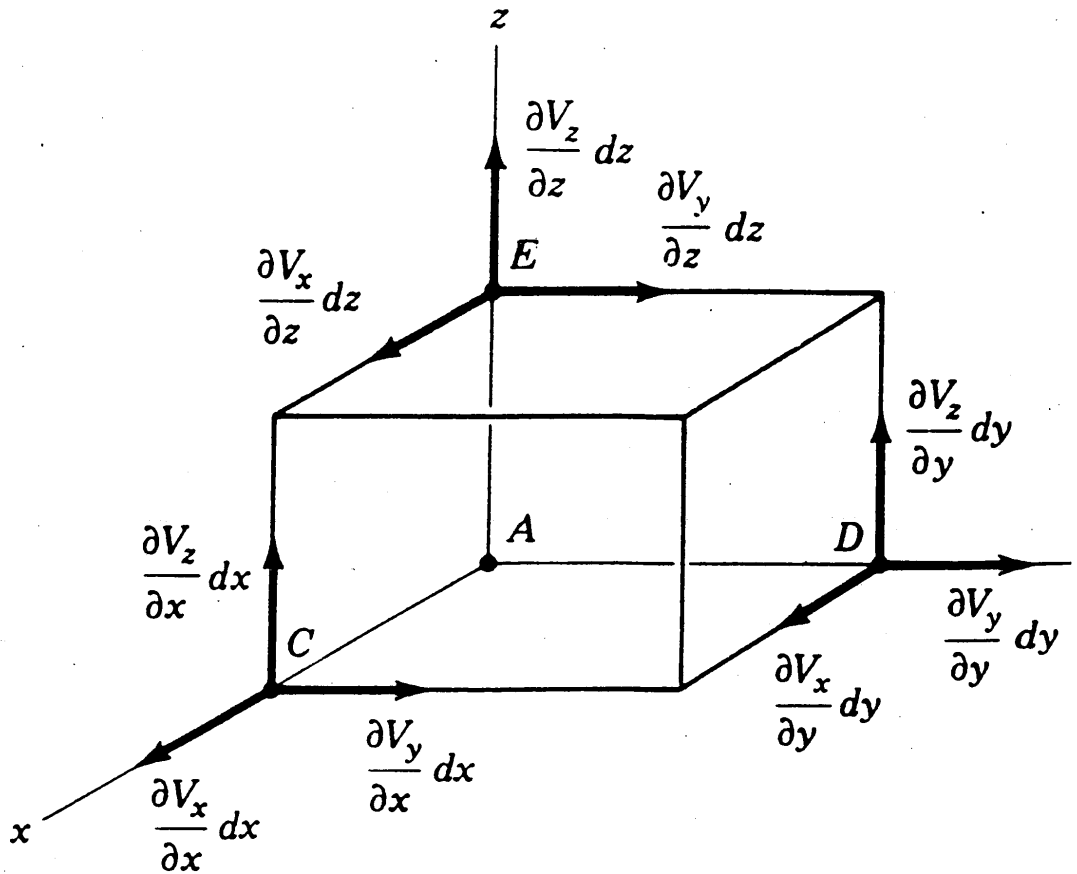
$$\vec{V}_C = \vec{V}_A + \frac{\partial \vec{V}}{\partial x} dx$$

$$(\vec{V}_C - \vec{V}_A) = \frac{\partial V_x}{\partial x} dx \hat{i} + \frac{\partial V_y}{\partial x} dx \hat{j} + \frac{\partial V_z}{\partial x} dx \hat{k}$$

$\frac{\partial V_x}{\partial x}$ ELONGATES \overline{AC}

$\frac{\partial V_z}{\partial x}$ ROTATES \overline{AC} ABOUT THE Y AXIS

$\frac{\partial V_y}{\partial x}$ ROTATES \overline{AC} ABOUT THE Z AXIS



$$\dot{\epsilon}_{xx} = \frac{\partial V_x}{\partial x}$$

$$\dot{\epsilon}_{yy} = \frac{\partial V_y}{\partial y}$$

$$\dot{\epsilon}_{zz} = \frac{\partial V_z}{\partial z}$$

$\angle DAE$

$$\dot{\gamma}_{yz} = \frac{\partial V_y}{\partial z} + \frac{\partial V_z}{\partial y}$$

$$\omega_x = \frac{1}{2} \left(\frac{\partial V_z}{\partial y} - \frac{\partial V_y}{\partial z} \right)$$

$\angle CAE$

$$\dot{\gamma}_{xz} = \frac{\partial V_x}{\partial z} + \frac{\partial V_z}{\partial x}$$

$$\omega_y = \frac{1}{2} \left(\frac{\partial V_x}{\partial z} - \frac{\partial V_z}{\partial x} \right)$$

$\angle CAD$

$$\dot{\gamma}_{xy} = \frac{\partial V_x}{\partial y} + \frac{\partial V_y}{\partial x}$$

$$\omega_z = \frac{1}{2} \left(\frac{\partial V_y}{\partial x} - \frac{\partial V_x}{\partial y} \right)$$

EQUATIONS OF MOTION

$$\rho \frac{DV_x}{Dt} = -\frac{\partial p}{\partial x} + \rho B_x + \frac{\partial \tau'_{xx}}{\partial x} + \frac{\partial \tau'_{yx}}{\partial y} + \frac{\partial \tau'_{zx}}{\partial z}$$

$$\rho \frac{DV_y}{Dt} = -\frac{\partial p}{\partial y} + \rho B_y + \frac{\partial \tau'_{xy}}{\partial x} + \frac{\partial \tau'_{yy}}{\partial y} + \frac{\partial \tau'_{zy}}{\partial z}$$

$$\rho \frac{DV_z}{Dt} = -\frac{\partial p}{\partial z} + \rho B_z + \frac{\partial \tau'_{xz}}{\partial x} + \frac{\partial \tau'_{yz}}{\partial y} + \frac{\partial \tau'_{zz}}{\partial z}$$

INCOMPRESSIBLE CONTINUITY

$$\frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} + \frac{\partial V_z}{\partial z} = 0$$

STRESS - STRAIN

$$\tau'_{xx} = 2\mu \frac{\partial V_x}{\partial x}$$

$$\tau'_{xy} = \tau'_{yx} = \mu \left(\frac{\partial V_x}{\partial y} + \frac{\partial V_y}{\partial x} \right)$$

$$\tau'_{yy} = 2\mu \frac{\partial V_y}{\partial y}$$

$$\tau'_{xz} = \tau'_{zx} = \mu \left(\frac{\partial V_x}{\partial z} + \frac{\partial V_z}{\partial x} \right)$$

$$\tau'_{zz} = 2\mu \frac{\partial V_z}{\partial z}$$

$$\tau'_{yz} = \tau'_{zy} = \mu \left(\frac{\partial V_y}{\partial z} + \frac{\partial V_z}{\partial y} \right)$$

NAVIER-STOKES EQUATIONS
FOR AN INCOMPRESSIBLE FLUID

$$\rho \frac{DV_x}{Dt} = -\frac{\partial p}{\partial x} + \rho B_x + \mu \left(\frac{\partial^2 V_x}{\partial x^2} + \frac{\partial^2 V_x}{\partial y^2} + \frac{\partial^2 V_x}{\partial z^2} \right)$$

$$\rho \frac{DV_y}{Dt} = -\frac{\partial p}{\partial y} + \rho B_y + \mu \left(\frac{\partial^2 V_y}{\partial x^2} + \frac{\partial^2 V_y}{\partial y^2} + \frac{\partial^2 V_y}{\partial z^2} \right)$$

$$\rho \frac{DV_z}{Dt} = -\frac{\partial p}{\partial z} + \rho B_z + \mu \left(\frac{\partial^2 V_z}{\partial x^2} + \frac{\partial^2 V_z}{\partial y^2} + \frac{\partial^2 V_z}{\partial z^2} \right)$$

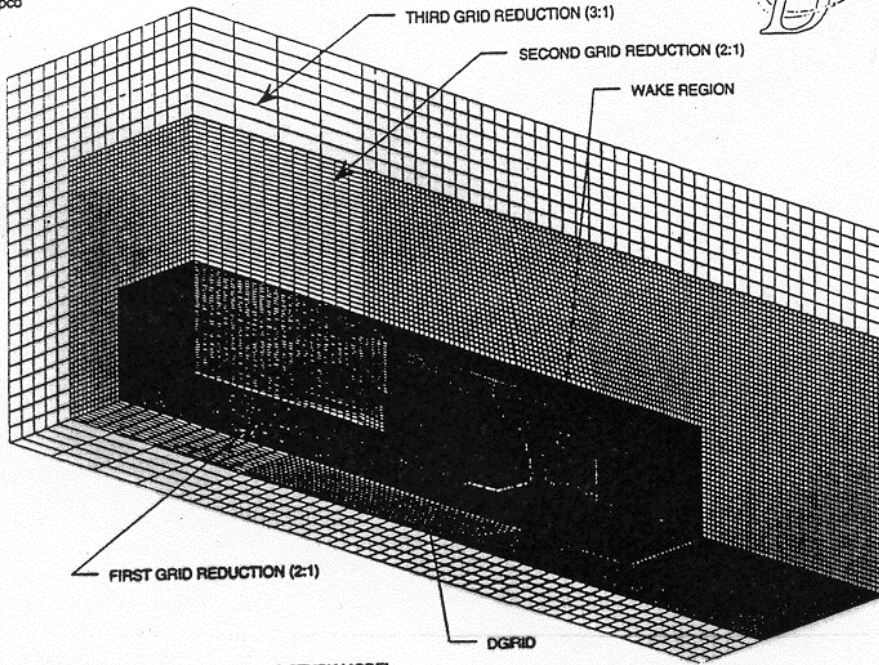
CONTINUITY: $\frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} + \frac{\partial V_z}{\partial z} = 0$

TO BE SOLVED FOR

$$V_x, V_y, V_z + p$$

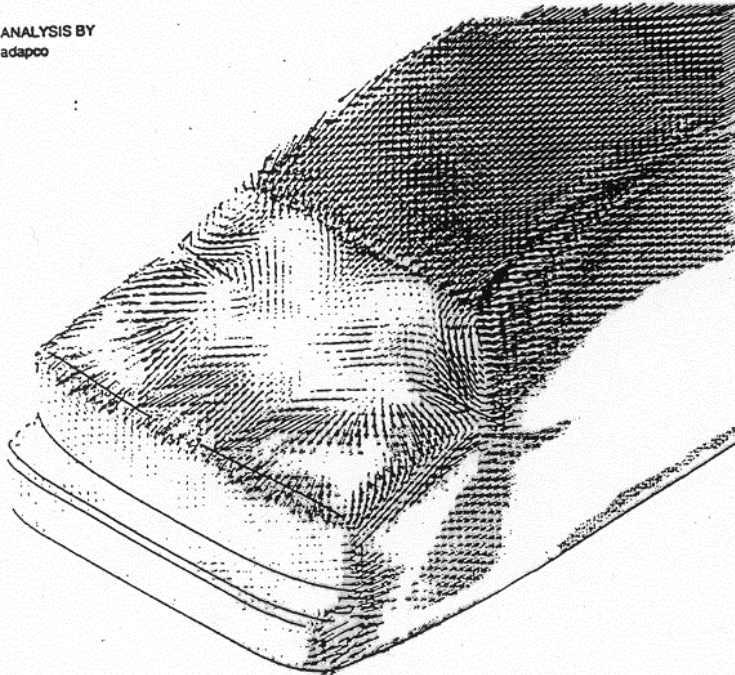
AS FUNCTIONS OF x, y, z, t

ANALYSIS BY
adapco



NOTCHBACK WIND TUNNEL AERODYNAMIC STUDY MODEL
COMPLETE MODEL DOMAIN

ANALYSIS BY
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02-Jul-93
MAGNITUDE VELOCITY
MS

LOCAL MAX= 53.46
LOCAL MIN= 0.0000E+00
"PRESENTATION GRID"

- 35.00
- 34.00
- 33.00
- 32.00
- 31.00
- 30.00
- 29.00
- 28.00
- 27.00
- 26.00
- 25.00
- 24.00
- 23.00
- 22.00
- 21.00
- 20.00
- 19.00
- 18.00
- 17.00
- 16.00
- 15.00

WIND TUNNEL AERODYNAMICS STUDY OF NOTCHBACK TEST SHAPE
KE RESULTS - KE TURBULENCE MODEL WITH LUD
VELOCITY MAGNITUDE NEAR THE VEHICLE

VIEW FROM REAR

NUMERICAL SOLUTION

restricting the momentum equation to Newtonian fluids for which the fluids stress is a linear function of the rate of deformation of the fluid - the change of velocity with distance.

$$\text{for 1 D, } \tau = \mu \frac{du}{dx}$$

$$\tau_{xx} = -2\mu \frac{\partial u}{\partial x} + \frac{2}{3}\mu(\nabla \vec{V})$$

$$\tau_{yy} = -2\mu \frac{\partial v}{\partial x} + \frac{2}{3}\mu(\nabla \vec{V})$$

$$\tau_{zz} = -2\mu \frac{\partial w}{\partial x} + \frac{2}{3}\mu(\nabla \vec{V})$$

$$\tau_{xy} = \tau_{yx} = -\mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)$$

$$\tau_{yz} = \tau_{zy} = -\mu \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)$$

$$\tau_{xz} = \tau_{zx} = -\mu \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right)$$

ENERGY EQUATION CONSERVATIVE INTEGRAL FORM

$$\text{First Law } Q = \Delta E + W = \Delta E + W_{\text{shaft}} + W_{\text{viscous}} + W_{\text{pressure}} + W_{\text{body}}$$

$$\text{Work} = \text{Force} \times \text{Velocity}$$

$$W_{\text{shaft}} = 0$$

$$\text{Work}_{\text{pressure}} = - \oint_A (p \, dA) \vec{V}$$

$$\text{Work}_{\text{body}} = \iiint_{\text{Vol}} (\rho \, f \, d \, \text{vol}) \vec{V}$$

$$\text{Work}_{\text{viscous}} = - \oint_A (\tau \, dA) \vec{V}$$

$$\text{Net Energy into control volume} = \oint_A (\rho \, V \, dA) \left(e + \frac{V^2}{2} \right)$$

$$\text{Change in energy inside the control volume} = \frac{\partial}{\partial t} \iiint_{\text{Vol}} \rho \left(e + \frac{V^2}{2} \right) d \, \text{vol}$$

$$\text{Heat addition} = \oint_A \vec{q} \, dA$$

$$\text{Internal energy, } U = c_v T$$

First Law $Q = \Delta E + W = \Delta E + W_{\text{shaft}} + W_{\text{viscous}} + W_{\text{pressure}} + W_{\text{body}}$

$$Q = \Delta E_{\substack{\text{net in} \\ \text{control} \\ \text{volume}}} + \Delta E_{\substack{\text{change in} \\ \text{control volume}}} + W_{\text{shaft}} + W_{\text{viscous}} + W_{\text{pressure}} + W_{\text{body}}$$

$$Q = \iint_A (\rho \vec{\nabla} \cdot d\mathbf{A}) \left(e + \frac{V^2}{2} \right) + \frac{\partial}{\partial t} \iiint_{\text{vol}} \rho \left(e + \frac{V^2}{2} \right) d \text{ vol} + \iint_A (\tau \cdot d\mathbf{A}) \vec{V} - \iint_A (p \vec{V}) \cdot d\mathbf{A} + \iiint_{\text{vol}} (\rho \mathbf{f} \cdot d \text{ vol}) \vec{V}$$

$$\frac{\partial}{\partial t} \rho \left(c_v T + \frac{V^2}{2} \right) = - \left(\nabla \rho \cdot \vec{\nabla} \left(c_v T + \frac{V^2}{2} \right) \right) - \nabla \cdot \mathbf{q} - \nabla \cdot p \vec{V} - \nabla \cdot (\boldsymbol{\tau} \cdot \vec{V}) + \rho (\mathbf{g} \cdot \vec{V})$$

$$\frac{\partial}{\partial t} \rho \left(c_v T + \frac{V^2}{2} \right) = - \left(\frac{\partial}{\partial x} u \rho \left(c_v T + \frac{V^2}{2} \right) + \frac{\partial}{\partial y} v \rho \left(c_v T + \frac{V^2}{2} \right) + \frac{\partial}{\partial z} w \rho \left(c_v T + \frac{V^2}{2} \right) \right)$$

$$- \left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z} \right) - \left(\frac{\partial}{\partial x} \rho u + \frac{\partial}{\partial y} \rho v + \frac{\partial}{\partial z} \rho w \right)$$

$$- \left(\frac{\partial}{\partial x} (\tau_{xx} u + \tau_{xy} v + \tau_{xz} w) + \frac{\partial}{\partial y} (\tau_{yx} u + \tau_{yy} v + \tau_{yz} w) + \frac{\partial}{\partial z} (\tau_{zx} u + \tau_{zy} v + \tau_{zz} w) \right)$$

$$\rho c_v \left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} \right) = - \left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z} \right) - T \left(\frac{\partial p}{\partial T} \right)_p \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

$$- \left(\tau_{xx} \frac{\partial u}{\partial x} + \tau_{yy} \frac{\partial v}{\partial y} + \tau_{zz} \frac{\partial w}{\partial z} \right) - \left(\tau_{xy} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) + \tau_{xz} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) + \tau_{yz} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \right)$$

EQUATION SUMMARY - 3D, viscous, variable density

CONTINUITY

$$\frac{\partial \rho}{\partial t} + \left(u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} \right) + \left(\rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + \rho \frac{\partial w}{\partial z} \right) = 0$$

MOMENTUM – x, y, z directions

$$\frac{\partial}{\partial t} \rho u = -\frac{\partial p}{\partial x} - \left(\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial y} + \rho w \frac{\partial u}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{yx} + \frac{\partial}{\partial z} \tau_{zx} \right) + \rho f_x$$

$$\frac{\partial}{\partial t} \rho v = -\frac{\partial p}{\partial y} - \left(\rho u \frac{\partial v}{\partial x} + \rho v \frac{\partial v}{\partial y} + \rho w \frac{\partial v}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xy} + \frac{\partial}{\partial y} \tau_{yy} + \frac{\partial}{\partial z} \tau_{zy} \right) + \rho f_y$$

$$\frac{\partial}{\partial t} \rho w = -\frac{\partial p}{\partial z} - \left(\rho u \frac{\partial w}{\partial x} + \rho v \frac{\partial w}{\partial y} + \rho w \frac{\partial w}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xz} + \frac{\partial}{\partial y} \tau_{yz} + \frac{\partial}{\partial z} \tau_{zz} \right) + \rho f_z$$

ENERGY

$$\rho c_v \left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} \right) = - \left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z} \right) - T \left(\frac{\partial p}{\partial T} \right)_p \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) - \left(\tau_{xx} \frac{\partial u}{\partial x} + \tau_{yy} \frac{\partial v}{\partial y} + \tau_{zz} \frac{\partial w}{\partial z} \right) - \left(\tau_{xy} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) + \tau_{xz} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) + \tau_{yz} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \right)$$

EQUATION SUMMARY - 3D, viscous, variable density

CONTINUITY

$$\frac{\partial \rho}{\partial t} + \left(u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} \right) + \left(\rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + \rho \frac{\partial w}{\partial z} \right) = 0$$

2D steady incompressible,
inviscid -> T = constant, adiabatic

MOMENTUM – x, y, z directions

$$\frac{\partial}{\partial t} \rho u = - \frac{\partial p}{\partial x} - \left(\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial y} + \rho w \frac{\partial u}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{yx} + \frac{\partial}{\partial z} \tau_{zx} \right) + \rho f_x$$

$$\frac{\partial}{\partial t} \rho v = - \frac{\partial p}{\partial y} - \left(\rho u \frac{\partial v}{\partial x} + \rho v \frac{\partial v}{\partial y} + \rho w \frac{\partial v}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xy} + \frac{\partial}{\partial y} \tau_{yy} + \frac{\partial}{\partial z} \tau_{zy} \right) + \rho f_y$$

$$\frac{\partial}{\partial t} \rho w = - \frac{\partial p}{\partial z} - \left(\rho u \frac{\partial w}{\partial x} + \rho v \frac{\partial w}{\partial y} + \rho w \frac{\partial w}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xz} + \frac{\partial}{\partial y} \tau_{yz} + \frac{\partial}{\partial z} \tau_{zz} \right) + \rho f_z$$

ENERGY

$$\rho c_v \left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} \right) = - \left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z} \right) - T \left(\frac{\partial p}{\partial T} \right)_p \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) - \left(\tau_{xx} \frac{\partial u}{\partial x} + \tau_{yy} \frac{\partial v}{\partial y} + \tau_{zz} \frac{\partial w}{\partial z} \right) - \left(\tau_{xy} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) + \tau_{xz} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) + \tau_{yz} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \right)$$

BOUNDARY LAYER Prandtl 1904

Divide a flow into two regions according to the forces that prevail

BOUNDARY LAYER

thin layer near wall

viscous forces as important as inertial forces

$\frac{\partial u}{\partial y}$ large, $\tau = \mu \frac{\partial u}{\partial y}$ very large

ignore traverse momentum equations

2-D incompressible boundary layer equations,

$$u \frac{\partial u}{\partial y} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{dp}{dx} + \frac{1}{\rho} \frac{\partial \tau_{yx}}{\partial y}$$

$$u \frac{\partial u}{\partial y} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{dp}{dx} + \frac{\mu}{\rho} \frac{\partial^2 u}{\partial y^2}$$

$$\frac{\partial u}{\partial x} + v \frac{\partial v}{\partial y} = 0$$

FREE STREAM

$\tau = 0, \mu = 0,$

Potential Flow

isentropic, frictionless

irrotational,

uniform and parallel

EQUATION SUMMARY - 3D, viscous, variable density

CONTINUITY

$$\frac{\partial \rho}{\partial t} + \left(u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} \right) + \left(\rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + \rho \frac{\partial w}{\partial z} \right) = 0$$

2D, Inviscid, steady, compressible

MOMENTUM – x, y, z directions

$$\frac{\partial}{\partial t} \rho u = - \frac{\partial p}{\partial x} - \left(\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial y} + \rho w \frac{\partial u}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{yx} + \frac{\partial}{\partial z} \tau_{zx} \right) + \rho f_x$$

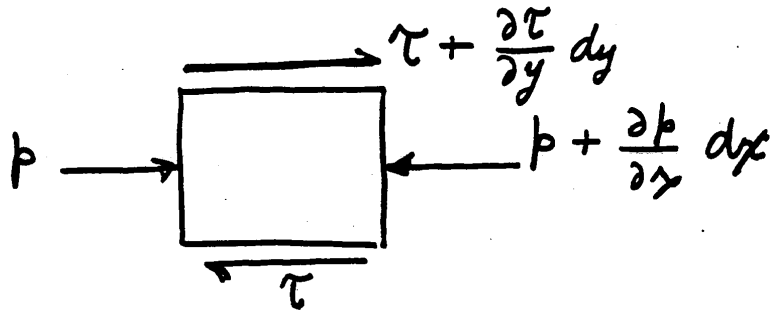
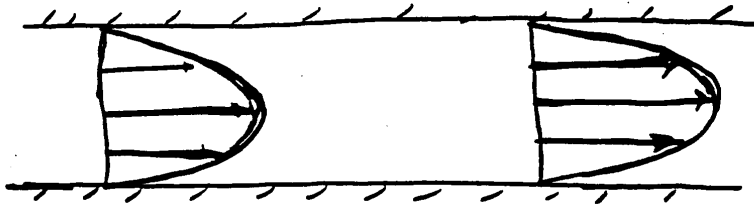
$$\frac{\partial}{\partial t} \rho v = - \frac{\partial p}{\partial y} - \left(\rho u \frac{\partial v}{\partial x} + \rho v \frac{\partial v}{\partial y} + \rho w \frac{\partial v}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xy} + \frac{\partial}{\partial y} \tau_{yy} + \frac{\partial}{\partial z} \tau_{zy} \right) + \rho f_y$$

$$\frac{\partial}{\partial t} \rho w = - \frac{\partial p}{\partial z} - \left(\rho u \frac{\partial w}{\partial x} + \rho v \frac{\partial w}{\partial y} + \rho w \frac{\partial w}{\partial z} \right) - \left(\frac{\partial}{\partial x} \tau_{xz} + \frac{\partial}{\partial y} \tau_{yz} + \frac{\partial}{\partial z} \tau_{zz} \right) + \rho f_z$$

ENERGY

$$\rho c_v \left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} \right) = - \left(\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + \frac{\partial q_z}{\partial z} \right) - T \left(\frac{\partial p}{\partial T} \right)_p \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) - \left(\tau_{xx} \frac{\partial u}{\partial x} + \tau_{yy} \frac{\partial v}{\partial y} + \tau_{zz} \frac{\partial w}{\partial z} \right) - \left(\tau_{xy} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) + \tau_{xz} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) + \tau_{yz} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \right)$$

PARALLEL FLOW



$$\Sigma F_x = p \, dy \, dz - \left(p + \frac{\partial p}{\partial x} dx \right) dy \, dz + \tau \, dx \, dz + \left(\tau + \frac{\partial \tau}{\partial y} dy \right) dx \, dz = \rho a_x \, dz$$

$$\rho \frac{DV_x}{Dt} = - \frac{\partial p}{\partial x} + \frac{\partial \tau}{\partial y}$$

$$\tau = \mu \frac{\partial V_x}{\partial y}$$

$$\rho \frac{DV_x}{Dt} = - \frac{\partial p}{\partial x} + \mu \frac{\partial^2 V_x}{\partial y^2}$$

$$\frac{DV_x}{Dt} = \frac{\partial V_x}{\partial t} + V_x \frac{\partial V_x}{\partial x} + V_y \frac{\partial V_x}{\partial y} = \frac{\partial V_x}{\partial t}$$

VISCOSITY - UNITS

$$\tau = \mu \frac{\partial v}{\partial y}$$

$$\mu = \tau / \partial v / \partial y$$

ENGLISH

$$\mu \sim \frac{\text{lb}/\text{ft}^2}{1/\text{sec}} = \frac{\text{lb sec}}{\text{ft}^2}$$

$$\text{lb} = \text{slug ft}/\text{sec}^2$$

$$\mu = \frac{\text{slug}}{\text{ft sec}}$$

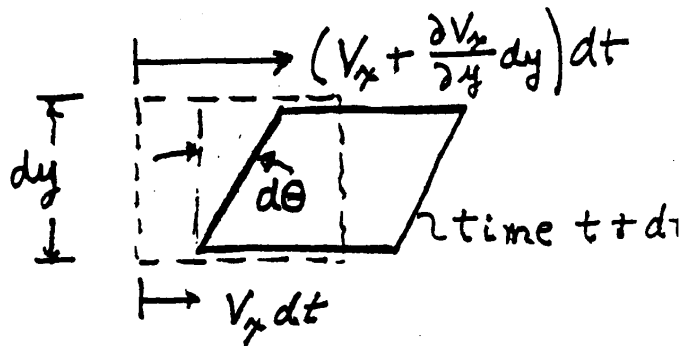
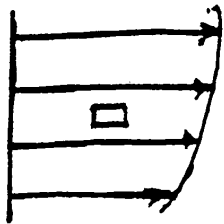
METRIC

$$\mu \sim \frac{\text{N}/\text{m}^2}{1/\text{sec}} = \frac{\text{N-sec}}{\text{m}^2}$$

$$\text{N} = \text{kg m}/\text{sec}^2$$

$$\mu \sim \frac{\text{kg}}{\text{m} \cdot \text{sec}}$$

STRESS + STRAIN IN A PARALLEL FLOW



$$\tan d\theta \cong d\theta = \frac{(V_x + \frac{\partial V_x}{\partial y} dy) dt - V_x dt}{dy}$$

$$\text{STRAIN} = \frac{d\theta}{dt} = \frac{\partial V_x}{\partial y}$$

STRESS \propto STRAIN RATE (NEWTONIAN FLUID)

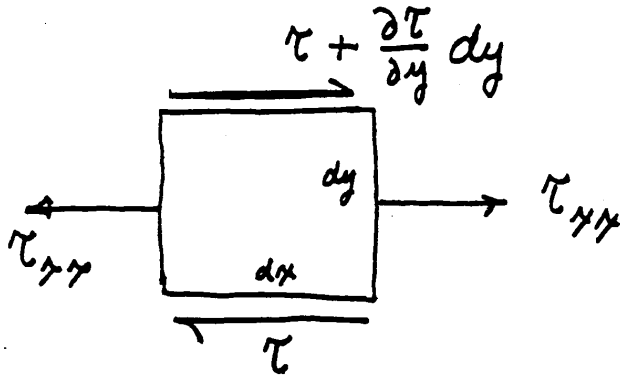
$$\tau_{xy} = \mu \frac{\partial V_x}{\partial y}$$

μ = COEFFICIENT OF VISCOSITY
PROPERTY OF THE FLUID

TABLE 1.2
Properties of common liquids at 1 atm and 20°C

Liquid	Viscosity μ		Kinematic viscosity $\nu = \mu/\rho$	
	kg / (m · s)	slug / (ft · s)	m ² / s	ft ² / s
Alcohol (ethyl)	1.2×10^{-3}	2.51×10^{-5}	1.51×10^{-6}	1.62×10^{-5}
Gasoline	2.9×10^{-4}	6.06×10^{-6}	4.27×10^{-7}	4.59×10^{-6}
Mercury	1.5×10^{-3}	3.14×10^{-5}	1.16×10^{-7}	1.25×10^{-6}
Oil (lubricant)	0.26	5.43×10^{-3}	2.79×10^{-4}	3.00×10^{-3}
Water	1.005×10^{-3}	1.67×10^{-5}	0.804×10^{-6}	8.65×10^{-6}

PARALLEL FLOW (STEADY)



FLOW IS
DRIVEN BY
SHEAR

$$\sum F_x = -\tau dx dy + \left(\tau + \frac{\partial \tau}{\partial y} dy\right) dx dy = \rho a \frac{dV}{dt} = 0$$

$$\frac{\partial \tau}{\partial y} = 0 \quad \tau = \text{CONSTANT}$$

$$\tau = \mu \frac{dV}{dy}$$

$$V = \frac{\tau}{\mu} y + C$$

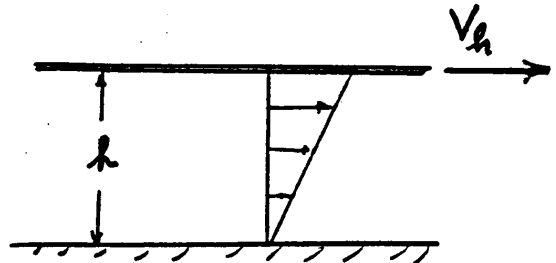
$$V(0) = 0 \quad C = 0$$

$$V(h) = V_h$$

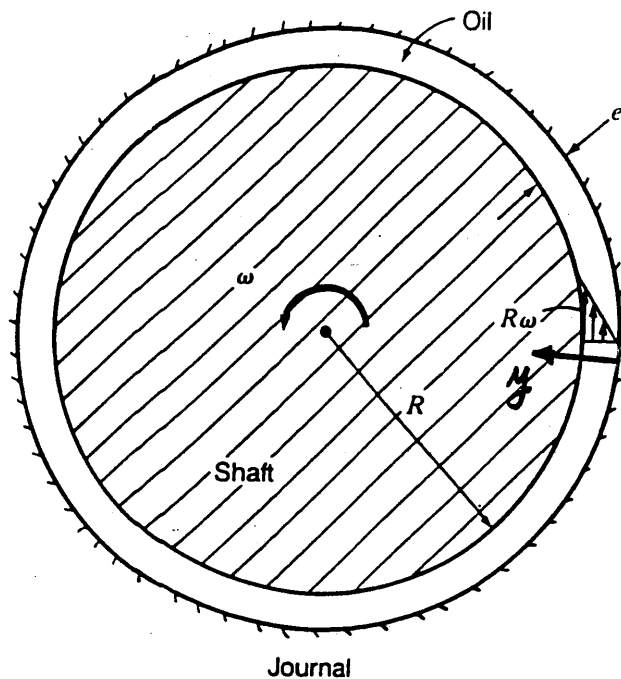
$$V_h = \frac{\tau}{\mu} h$$

$$\tau = \mu \frac{V_h}{h}$$

$$V = V_h \frac{y}{h}$$



ROTATING SHAFT



$$\tau = \mu \frac{\partial v}{\partial y} = \mu \frac{R\omega - 0}{e} = \mu \frac{R\omega}{e}$$

$$T_{\text{TORQUE}} = R(\tau 2\pi R l)$$

Oil $\mu = 5.43 \times 10^{-3} \frac{\text{SLUG}}{\text{ft} \cdot \text{s}}$

$$R = 3''$$

$$e = 0.1''$$

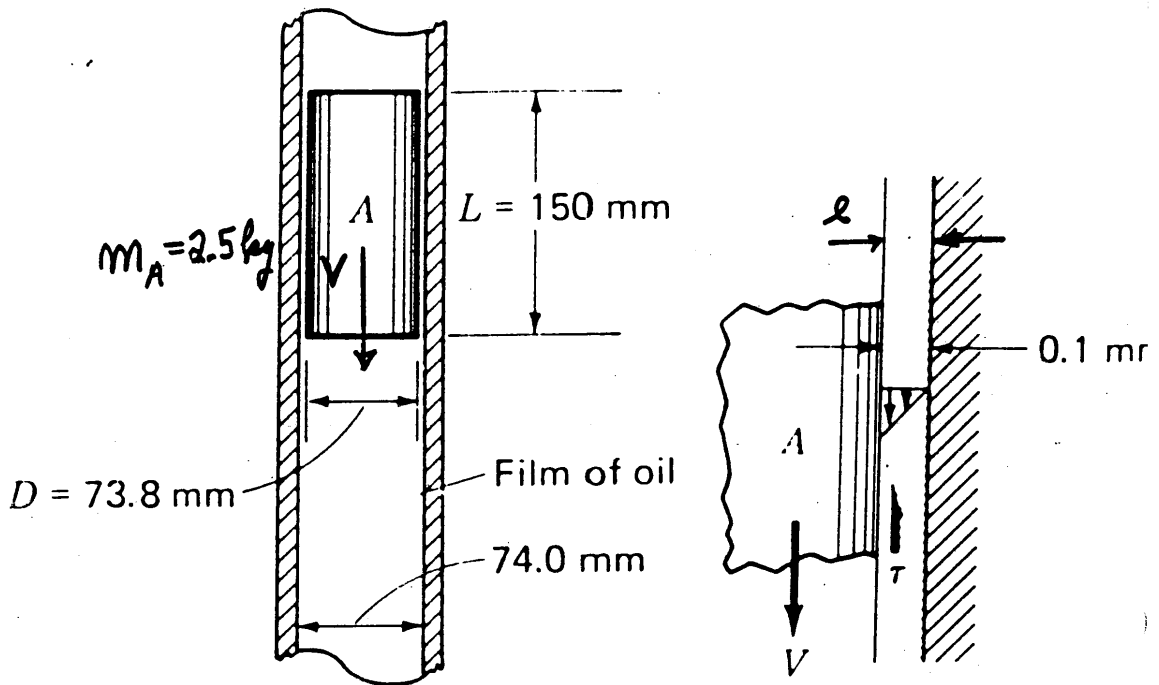
RPM = 1000 $\omega = 1000 \frac{2\pi}{60} = 104.7 \frac{\text{rad}}{\text{s}}$

$$\tau = 5.43 \times 10^{-3} \frac{(3/12) 104.7}{(0.1/12)} = 17.06 \text{ lb/ft}^2$$

$$F = \tau 2\pi R l = 17.06 (2\pi)(3/12)(1\text{ft}) = 26.8 \text{ lb}$$

$$T = R F = 6.7 \text{ ft} \cdot \text{lb}$$

EXAMPLE 1.1



What is the terminal velocity of the cylinder?

$$\tau = \mu \frac{\partial V}{\partial y} = \mu \frac{V}{\ell}$$

$$\mu = 7 \times 10^{-3} \frac{\text{N} \cdot \text{s}}{\text{m}^2}$$

$$\sum F_z = \tau \pi D L - W = 0$$

$$\mu \frac{V}{\ell} \pi D L = W$$

$$V = \frac{\ell W}{\mu \pi D L} = \frac{.0001 (2.5)(9.81)}{7 \times 10^{-3} \pi (.0738)(.150)}$$

$$= 10.07 \text{ m/s}$$