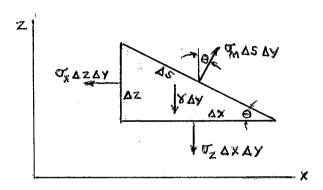
## **Equations for Frictionless Flows**

Pressure in a frictionless flow – no shear stresses



Equilibrium with Normal Stress Forces

$$\sum F_x = \sigma_n \Delta s \Delta y \sin \theta - \sigma_x \Delta z \Delta y = \rho \Delta \forall a_x$$
$$\sum F_z = \sigma_n \Delta s \Delta y \cos \theta - \sigma_z \Delta x \Delta y - \gamma \Delta \forall = \rho \Delta \forall a_z$$

$$\Delta \forall = \Delta x \Delta z \Delta y / 2$$
 and  $\Delta x = \Delta s \cos \theta$ ,  $\Delta z = \Delta s \sin \theta$ 

$$\sigma_n - \sigma_x = \rho \Delta x a_x / 2$$

$$\sigma_n - \sigma_z - \gamma \Delta z / 2 = \rho \Delta z a_z / 2$$

$$\Delta x \to 0, \Delta z \to 0 \text{ gives}$$

$$\sigma_n = \sigma_x = \sigma_z = -p$$

Stresses in a frictionless flow only involve the pressure. All the normal stresses are equal to negative the pressure

Euler's Equation: 
$$\rho \frac{D\vec{V}}{Dt} = -\nabla p + \rho \vec{g}$$

Component Equations:

$$\rho(\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + w\frac{\partial u}{\partial z}) = -\frac{\partial p}{\partial x} + \rho g_x$$

$$\rho(\frac{\partial v}{\partial t} + u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y} + w\frac{\partial v}{\partial z}) = -\frac{\partial p}{\partial y} + \rho g_y$$

$$\rho(\frac{\partial w}{\partial t} + u\frac{\partial w}{\partial x} + v\frac{\partial w}{\partial y} + w\frac{\partial w}{\partial z}) = -\frac{\partial p}{\partial z} + \rho g_z$$

Example Given the steady two dimensional velocity field, u=cx and v=-cy, find the pressure field for steady, incompressible, frictionless flow where the x axis is inclined upward at an angle  $\theta$  to the horizontal.

Continuity equation

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = c + (-c) = 0$$

Component momentum equations

$$\rho(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}) = -\frac{\partial p}{\partial x} + \rho g_x$$
$$\rho(u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y}) = -\frac{\partial p}{\partial y} + \rho g_y$$

which become

office
$$\rho[cx(c) - cy(0)] = -\frac{\partial p}{\partial x} - \rho g \sin \theta$$

$$\rho[cx(0) - cy(-c)] = -\frac{\partial p}{\partial y} - \rho g \cos \theta$$

$$\frac{\partial p}{\partial x} = -\rho c^2 x - \rho g \sin \theta$$

$$\frac{\partial p}{\partial y} = -\rho c^2 y - \rho g \cos \theta$$

$$p = -\frac{1}{2}\rho c^2 x^2 - \rho g x \sin \theta + e(y)$$

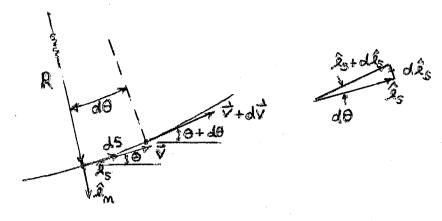
$$p = -\frac{1}{2}\rho c^2 y^2 - \rho g y \cos \theta + f(x)$$

$$p = p_0 - \frac{1}{2}\rho c^2 x^2 - \frac{1}{2}\rho c^2 y^2 - \rho g x \sin \theta - \rho g y \cos \theta$$

 $p_0$  = pressure at the origin.

## Bernoulli's equation

Steady, incompressible, frictionless flow along a streamline



$$\rho \frac{D\vec{V}}{Dt} = \rho V \frac{\partial \vec{V}}{\partial s} = -\nabla p + \rho \vec{g}$$

Velocity vector =  $\vec{V} = V\hat{e}_s$  $\hat{e}_s$  is a unit vector tangent to the streamline.

$$\partial \vec{V} / \partial s = (\partial V / \partial s)\hat{e}_s + V(\partial \hat{e}_s / \partial s)$$

Magnitude of  $d\hat{e}_s = d\theta$ 

Direction of  $d\hat{e}_s = -\hat{e}_n$  (normal direction)

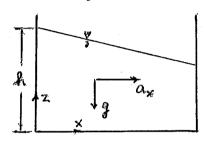
 $d\hat{e}_s / ds = -(d\theta / ds)\hat{e}_n = -\hat{e}_n / R$  since  $d\theta / ds = 1 / R$ R is the radius of curvature of the streamline

$$\rho V(\frac{\partial V}{\partial s}\hat{e}_s - \frac{V}{R}\hat{e}_n) = -\frac{\partial p}{\partial s}\hat{e}_s - \frac{\partial p}{\partial n}\hat{e}_n - \rho g\sin\theta\hat{e}_s - \rho g\cos\theta\hat{e}_n$$
$$\frac{\partial p}{\partial s} + \rho V\frac{\partial V}{\partial s} + \rho g\sin\theta = 0 \qquad \qquad \frac{\partial p}{\partial n} = \rho \frac{V^2}{R} - \rho g\cos\theta$$

$$p + \rho \frac{V^2}{2} + \rho gz = cons \tan t$$
 for a given streamline.

## Fluids Under Constant Acceleration

Fluid accelerating horizontally in the x direction Start up motions have subsided - all the liquid in the tank is at the same velocity



$$\rho a_x = -\frac{\partial p}{\partial x}$$

$$p = -\rho a_x x + e(z)$$

$$\partial p / \partial z = -\rho g \text{ in the vertical } z$$

$$p = -\rho gz + f(x)$$

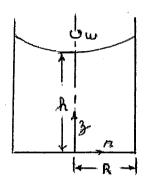
$$p = p_0 - \rho a_x x - \rho gz$$

 $p_0$  = the pressure at the origin

Surface of the liquid is at atmosphere pressure

$$p_a = p_0 - \rho a_x x - \rho g z$$
  
For x=0 and y=0:  $p_0 = p_a + \rho g h$   
 $z = h - (a_x / g) x$  for the surface (slope =  $-(a_x / g)$ )

**Example** A cylindrical tank, partially filled with a liquid, is placed on a turn table and rotated about its vertical centerline. What is the shape of the liquid surface which is exposed to the atmosphere since the tank is open at the top?



**Rotating Tank** 

Hydrostatic equation in the vertical direction

$$\partial p / \partial z = -\rho g$$
  $p = -\rho gz + f(r)$ 

In the radial direction:  $\partial p / \partial n = \rho V^2 / R$ 

$$\frac{\partial p}{\partial r} = \rho \frac{V^2}{r} = \rho \frac{(r\omega)^2}{r} = \rho \omega^2 r \qquad p = \rho \omega^2 r^2 / 2 + e(z)$$

Comparing the two solutions

$$p = p_0 + \rho \omega^2 r^2 / 2 - \rho gz$$

 $p_0$  = pressure at the origin of the coordinate system.

Surface is at the atmospheric pressure

$$p_a = p_0 + \rho \omega^2 r^2 / 2 - \rho g z$$

At r=0: 
$$p_a = p_0 - \rho g h$$

$$z = h + \frac{1}{2} \frac{\omega^2}{g} r^2$$