## COOLING TOWER SPREADSHEET DETAILS

Details of the Excel Spreadsheet are presented here. There are five sections, as follows:
Section 1 Laboratory Data
Data from the Laboratory Data Sheet are entered into the spreadsheet in the same order as they appear on the Data Sheet. Some parameters of the column operation are then calculated.

## Section 2 NTU Calculation

An analytical calculation of the NTU's is performed using a $2^{\text {nd }}$ order regression fit for the water line. The HTU's and $\mathrm{K}_{\mathrm{y}} \mathrm{a}$ 's are also calculated.

## Section 3 Evaporation Rate

The rate of evaporation is calculated.

## Section 4 Khodaparast's NTU Calculation

This section uses the analytical integration of Khodaparast. This integration utilizes a different regression fit from that in Section 2.

## Section 5 Summary

This section summarizes some of the results of the previous calculations.
A "Test Run" is included which serves as basis for copying all of the equations over into the adjacent columns. Data entires are shown in parenthese ( ) and calculation results are shown in brackets.

| Cell | Cell Entry | Notes and Equation Numbers | Test Run Entries o Results |
| :---: | :---: | :---: | :---: |
| A1 | Analysis of Cooling Tower Data |  |  |
| A2 | Damper Position = Fill it in here |  |  |
| A3 | Date due Fill it in here |  |  |
| A4 | See Word Spreadsheet File |  |  |
| A5 | for details. |  |  |
| A6 | \# = Symbol for humidity |  |  |
| A7 | Laboratory Data | Underline it or put a dashed line in Cell A8. |  |
| B7 |  |  |  |
| A8 | A dashed line below the title in A7 |  |  |
| B8 | Test Run |  |  |
| A9 | $\mathrm{H}_{2} \mathrm{O}$ rate, liters/min |  |  |
| B9 | A data entry |  | (10.5) |
| A10 | Hot water tank temp, ${ }^{\circ} \mathrm{C}$ |  |  |
| B10 | A data entry |  |  |
| A11 | Manometer Press. Drop, Inches of $\mathrm{H}_{2} \mathrm{O}$ |  |  |
| B11 | A data entry |  | (19.5646) |
| A12 | $\mathrm{T}_{\text {xa }}$, Inlet water, ${ }^{\circ} \mathrm{C}$ |  |  |
| B12 | A data entry |  | (43.3) |
| A13 | $\mathrm{T}_{\text {xb }}$, Outlet water, ${ }^{\circ} \mathrm{C}$ |  |  |
| B13 | A data entry |  | (22.5) |
| A14 | $\mathrm{T}_{\mathrm{yb}}$, Inlet air dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |
| B14 | A data entry |  | (21.0) |
| A15 | $\mathrm{T}_{\text {wbb }}$, Inlet air wet bulb, ${ }^{\circ} \mathrm{C}$ |  |  |


| B15 | A data entry |  | (14.1) |
| :---: | :---: | :---: | :---: |
| A16 | $\mathrm{T}_{\text {ya }}$, Outlet air dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |
| B16 | A data entry |  | (44.0) |
| A17 |  | This is a blank row. |  |
| B17 |  |  |  |
| A18 | $\mathrm{T}_{\mathrm{xa}}$, Inlet water, ${ }^{\circ} \mathrm{F}$ |  |  |
| B18 | $=(\mathrm{B} \$ 12+40)^{*} 1.8-40$ | Equation to convert ${ }^{\circ} \mathrm{C}$ to ${ }^{\circ} \mathrm{F}$ | [109.9] |
| A19 | $\mathrm{T}_{\mathrm{xb}}$, Outlet water, ${ }^{\circ} \mathrm{F}$ |  |  |
| B19 | $=(\mathrm{B} \$ 13+40)^{*} 1.8-40$ | Equation to convert ${ }^{\circ} \mathrm{C}$ to ${ }^{\circ} \mathrm{F}$ | [72.5] |
| A20 | $\mathrm{T}_{\mathrm{yb}}$, Inlet air dry bulb, ${ }^{\circ} \mathrm{F}$ |  |  |
| B20 | $=(B \$ 14+40)^{*} 1.8-40$ | Equation to convert ${ }^{\circ} \mathrm{C}$ to ${ }^{\circ} \mathrm{F}$ | [69.8] |
| A21 | $\mathrm{T}_{\text {wbb }}$, Inlet air wet bulb, ${ }^{\circ} \mathrm{F}$ |  |  |
| B21 | $=(\mathrm{B} \$ 15+40)^{*} 1.8-40$ | Equation to convert ${ }^{\circ} \mathrm{C}$ to ${ }^{\circ} \mathrm{F}$ | [57.4] |
| A22 | $\mathrm{T}_{\mathrm{ya}}$, Outlet air dry bulb, ${ }^{\circ} \mathrm{F}$ |  |  |
| B22 | $=(\text { B } 16+40)^{*} 1.8-40$ | Equation to convert ${ }^{\circ} \mathrm{C}$ to ${ }^{\circ} \mathrm{F}$ | [111.2] |
| A23 |  | This is a blank row. |  |
| B23 |  |  |  |
| A24 | $\mathrm{G}_{\mathrm{x},}$, lb $\mathrm{H}_{2} \mathrm{O} /\left(\mathrm{h}, \mathrm{ft}^{\wedge} 2\right)$ |  |  |
| B24 | = B9*0.035315*62.4*60 | Liters $/ \mathrm{min} \times 0.35315 \mathrm{ft}^{3} / \mathrm{liter} \times 62.4 \mathrm{lb} / \mathrm{ft}^{3} \times 60$ $\mathrm{min} / \mathrm{hr}$ | [1388] |
| A25 | \# b , lb $\mathrm{H}_{2} \mathrm{O} / \mathrm{lb} \mathrm{DA}$ |  |  |
| B25 | $\#_{\mathrm{b}}=\#_{\text {wb }}+0.000231(\mathrm{~B} 21-\mathrm{B} 20)$ | See details below | [0.0070] |

The following equations are involved in calculating $\#_{\mathrm{wb}}$ :
$\#_{w b}=\frac{M_{A} P_{A}^{\prime}}{M_{B}\left(1-P_{A}^{\prime}\right)}=\frac{M_{A}}{M_{B}}-1$ Equation (23.3) in MS\& H
where $\quad M_{A}=18.02 \quad$ Molecular weight of water
and $\quad P_{A}^{\prime}=\exp { }^{1 \rightarrow} 3036-\frac{6869.592}{T_{w b}+376.666}$ Antoine's Equation

| A26 | $\mathrm{H}_{\mathrm{yb}}$, Btu/lb DA |  |  |
| :---: | :---: | :---: | :---: |
| B26 | $=0.24 *$ B20 + B25*1075.8+0.45*(B20-32) |  | [24.432] |
| A27 | $\mathrm{V}_{\mathrm{H}}, \mathrm{ft}^{3} / \mathrm{lb}$ DA |  |  |
| B27 | Equation (23.7a) | Note that T here is in ${ }^{\circ} \mathrm{R}$ | [13.487] |
| A28 | Vol. air rate, $\mathrm{ft}^{3} / \mathrm{h}$ |  |  |
| B28 | $=(1.3328 * \mathrm{LN}(\mathrm{B} 11)+5.9569) * 3600$ | Regression fit of Pitot Tube Calibration | [35713] |
| A29 | $\mathrm{G}^{\prime}, \mathrm{lb} \mathrm{DA} /\left(\mathrm{h}, \mathrm{ft}^{2}\right)$ |  |  |
| B29 | =B28/B27 | Entering air rate/v $\mathrm{v}_{\mathrm{H}}$ | [2648] |
| A30 | $\mathrm{s}=\mathrm{G}_{x} \mathrm{c}_{L} / \mathrm{G}^{\prime}, \mathrm{Btu} /\left(\mathrm{lb} \mathrm{DA},{ }^{\circ} \mathrm{F}\right)$ |  |  |
| B30 | =B24/B29 | Operating Line Slope Equation(12) | [0.5243] |
| A31 |  | This row is blank |  |
| B31 |  |  |  |
| A32 | Analytical Integration | Underline it or put a dashed line in cell A32 |  |
| B32 |  |  |  |
| A33 | ================ |  |  |
| B33 | This cell is blank |  |  |


| A34 | $\mathrm{s}=\mathrm{G}_{x} \mathrm{C}_{L} / \mathrm{G}^{\prime}, \mathrm{Btu} /\left(\mathrm{lb} \mathrm{DA},{ }^{\circ} \mathrm{F}\right)$ |  |  |
| :---: | :---: | :---: | :---: |
| B34 | =B30 |  | [0.5243] |
| A35 | gamma |  |  |
| B35 | 100.081 |  | [100.081] |
| A36 | alpha |  |  |
| B36 | -2.52683 |  | $\begin{aligned} & \hline[- \\ & \text { 2.52683] } \\ & \hline \end{aligned}$ |
| A37 | beta |  |  |
| B37 | 0.0022464 |  | $\begin{aligned} & {[0.02246} \\ & 4] \end{aligned}$ |
| A38 | $\mathrm{T}_{\mathrm{xb}}$, ${ }^{\circ} \mathrm{F}$ |  |  |
| B38 | =B19 |  | [72.5] |
| A39 | $\mathrm{H}_{\text {yb }}$, Btu/lb DA |  |  |
| B39 | =B26 |  | [24.432] |
| A40 | f |  |  |
| B40 | =B26-B34*B38 | $\mathrm{f}=\mathrm{H}_{\mathrm{yb}}-\mathrm{s} \mathrm{T}_{\mathrm{xb}} \quad$ Equation (14) | [-13.581] |
| A41 | $a=$ gamma -f |  |  |
| B41 | =B35-B40 | Equation (16) | [113.662] |
| A42 | $\mathrm{b}=$ alpha -s |  |  |
| B42 | =B36-B34 | Equation (17) | [-3.051] |
| A43 | c = beta |  |  |
| B43 | =B37 | Equation (18) | $[0.02246$ |
| A44 | sart delta |  |  |
| B44 | =SQRT ((4*B41*B43)-B42^2) | Square Root of (4ac-b ${ }^{2}$ ) | [0.951] |
| A45 | $\mathrm{T}_{\text {xa }},{ }^{\circ} \mathrm{F}$ |  |  |
| B45 | =B18 |  | [109.9] |
| A46 | Numer1 |  |  |
| B46 | =2*B43*B38+B42 | Numerator of $1^{\text {st }} \mathrm{tan}^{-1}$ term of Equation (20) | [0.206] |
| A47 | Numer2 |  |  |
| B47 | =2*B43*B45+B42 | Numerator of $2^{\text {nd }} \tan ^{-1}$ term of Equation (20) | [1.888] |
| A48 | NTU |  |  |
| B48 | $\begin{aligned} & =\text { B34*2/B44*(ATAN2(B44,B47)- } \\ & \text { ATAN2(B44,B46)) } \end{aligned}$ | Equation (20) | [0.983] |
| A49 |  | This row is blank. |  |
| B49 |  |  |  |
| A50 | HTU, ft |  |  |
| B50 | =6/B48 | Equation (21) where $\mathrm{Z}_{\mathrm{T}}=6 \mathrm{ft}$ | [6.106] |
| A51 | $\mathrm{K}_{\mathrm{y}} \mathrm{a}, \mathrm{lb} \mathrm{DA} /\left(\mathrm{h}, \mathrm{ft}^{3}\right)$ |  |  |
| B51 | = B29/B50 | Equation (24) | [433.7] |
| A52 |  | This row is blank |  |
| B52 |  |  |  |
| A53 | Evaporation Rate | Underline it or put a dashed line in cell A54 |  |
| B53 |  |  |  |
| A54 | ============= |  |  |
| B54 |  |  |  |
| A55 | $\mathrm{T}_{\mathrm{yb}}$ |  |  |
| B55 | =B20 |  | [69.8] |
| A56 | $\mathrm{T}_{\text {wbb }}$ |  |  |
| B56 | = ${ }^{\text {2 }} 1$ |  | [57.4] |
| A57 | \#b |  |  |
| B57 | = ${ }^{\text {2 }}$ 25 |  | [0.0070] |
| A58 | $\mathrm{H}_{\mathrm{yb}}$ |  |  |
| B58 | =B26 |  | [24.432] |
| A59 | Cal'd $\mathrm{H}_{\mathrm{ya}}$, Btu/lb DA |  |  |


| B59 | = $\mathrm{B} 58+\mathrm{B} 30 *$ (B18-B19) | $\mathrm{H}_{\mathrm{ya}}=\mathrm{H}_{\mathrm{yb}}+\mathrm{s}\left(\mathrm{T}_{\mathrm{xa}}-\mathrm{T}_{\mathrm{xb}}\right)$ | [0.01563] |
| :---: | :---: | :---: | :---: |
| A60 | Cal'd \#, lb H2O/Lb DA |  |  |
| B60 | =(B59-0.24*B22)/(1075.8+0.45(B22-32)) | $\#_{\mathrm{a}}=\left(\mathrm{H}_{\mathrm{ya}}-0.24 \mathrm{~T}_{\mathrm{y}} \mathrm{l} /\left(1075.8+0.45\left(\mathrm{~T}_{\mathrm{ya}}-32\right)\right)\right.$ | [0.01563] |
| A61 | $\mathrm{G}_{\mathrm{xe}}=\mathrm{G}^{\prime}{ }^{\prime}\left(\#_{\mathrm{a}}-\#_{\mathrm{b}}\right)$ | This is the evaporation, $\mathrm{lb} \mathrm{H}_{2} \mathrm{O} /\left(\mathrm{h}, \mathrm{ft}^{2}\right)$ |  |
| B61 | =B29**(B60-B25) |  | [22.783] |
| A62 | Percent Evaporation |  |  |
| B62 | =B61/B24*100 | $\left(\mathrm{G}_{\mathrm{x}} / \mathrm{G}_{\mathrm{x}}\right)^{*} 100$ | [1.641] |

Enter all of your data, beginning in Column C and copy all of the equations from Column B across. Retain the "test run" in Column B.

