

This problem deals with experiments performed in a

laboratory on adsorption of water from air in a bed filled with silica gel (length $L = 60$ cm). Measured concentration profiles are shown in Fig. 4 for various times after the initial time $t = 0$, with $x =$ distance along bed. You may assume that $c(L,t) = 0$ for $t \leq 2$ h. Details of the experiment are as follows:

$$u_0 = \text{superficial gas velocity} = 13.1 \text{ cm/s};$$

$$y_0 = \text{water mole fraction in entering gas} = 5210 \times 10^{-6};$$

$$T = 20^\circ\text{C};$$

$$P = 3.0 \text{ atm};$$

$$\rho_{\text{bed}} = 0.30 \text{ g silica gel/cm}^3 \text{ bed volume}$$

The break-point time t_b is defined by the criterion $c(L,t_b) = 0.10 c_0$.

The experiment was interrupted at five hours and therefore there is insufficient data to determine the saturation capacity of the bed by time integration. Figure 5 will allow you to determine w_{sat} by alternate means.

- (10 points) What is the saturation capacity of the bed w_{sat} in g water/g silica gel?
- (30 points) What is the unused capacity of the silica gel (in terms of equivalent bed length) at the break-point?
- (10 points) Estimate the break-point time for a longer bed length of 100 cm, all other conditions being equal.

Data: vapor pressure of water

$T(^{\circ}\text{C})$	$P_{\text{H}_2\text{O}}^{\text{sat}}$ (mm Hg)
20	19.8
30	31.8
40	55.3

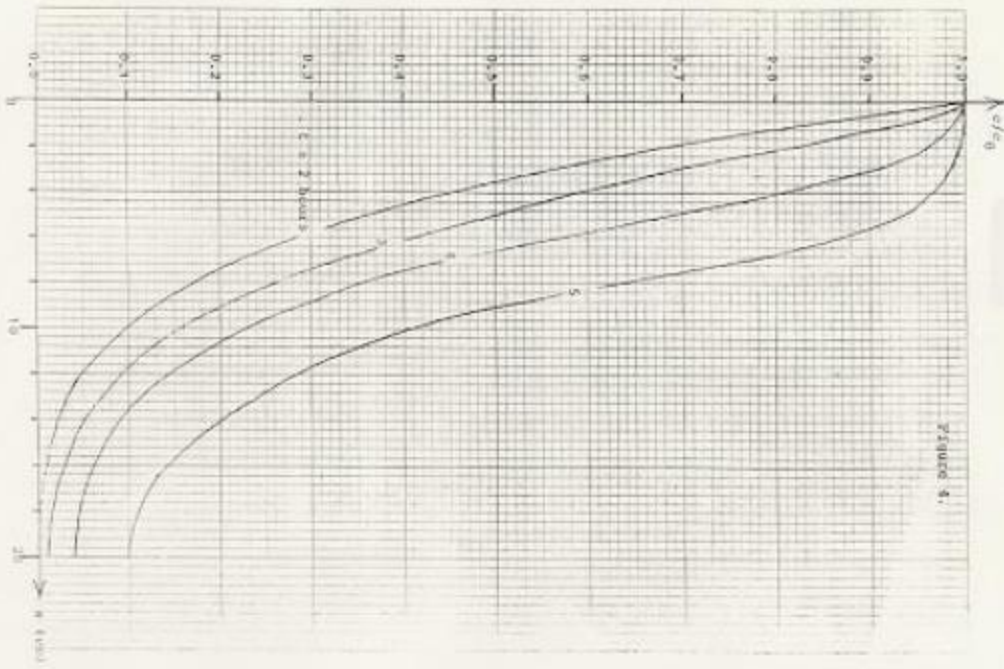


Figure 5.

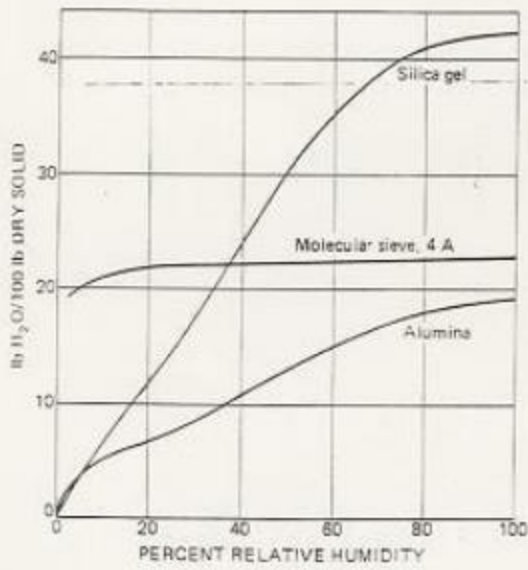


Figure 24-3 Adsorption isotherms for water in air at 20 to 50°C.

HR

(a) Incoming air: $P_{H_2O} = y_{H_2O} P$
 $= (5210 \cdot 10^{-6})(3 \text{ atm} \times \frac{760 \text{ mmHg}}{1 \text{ atm}})$
 $= 11.88 \text{ mmHg}$

at 0°C $P_{H_2O}^{sat} = 19.8 \text{ mmHg}$. Then

$$H_R = (100\%) \frac{P_{H_2O}}{P_{H_2O}^{sat}} = (100\%) \frac{11.88}{19.8} = 60.0\%$$

From Fig. 5, $W_{sat} = \frac{35.2 \text{ lb H}_2\text{O}}{100 \text{ lb air/gal}} = \boxed{0.352 \frac{\text{g H}_2\text{O}}{\text{g air/gal}}}$

(b) Solute in:

$$(F_A)_{in} = \left(\frac{\text{mass}}{\text{area} \cdot \text{time}} \right) \text{ solute in } c_0$$

$$= U_0 \cdot \left(\text{total cross-sectional area} \right) \cdot c_0 \cdot M_A$$

$$= (13.1 \text{ cm/s}) \left[\frac{(3 \times 10^{13} \text{ Pa})}{(8.314 \frac{\text{J}}{\text{mol} \cdot \text{K}})(293.15 \text{ K})} \times \frac{1 \text{ m}^3}{10^6 \text{ cm}^3} \right] \left(\frac{5210}{10^6} \right)$$

$$\rightarrow \times \frac{18.015 \text{ g solute}}{\text{mol solute}} \times \frac{3600 \text{ s}}{1 \text{ h}}$$

$$= 0.552 \frac{\text{g solute}}{\text{cm}^2 \cdot \text{h}}$$

Solute out: $c(L, t)$

$$(F_A)_{out} = U_0 c M_A = (U_0 c_0 M_A) (c/c_0) = (F_A)_{in} (c/c_0)$$

Solute accumulated: Solute accumulated in bed/area in time interval $(t, t+dt)$ is $[(F_A)_{in} - (F_A)_{out}] dt$
 $= (F_A)_{in} \left[1 - \frac{c(L, t)}{c_0} \right] dt$

Solute accumulated/area from time 0 to t is given by

$$\text{solute adsorbed/area} = (F_A)_{in} \int_0^t \left[1 - \frac{c(L,t')}{c_0} \right] dt'$$

Read off value of $c(L,t)$ from graph. Prepare table. Break-point time t_b is time at which $c(L,t_b) = 0.10 c_0$, so $t_b = 5$ h.

t (h)	$\frac{c(L,t)}{c_0}$	$1 - \frac{c(L,t)}{c_0}$	Contrib. to integral $\int_0^t (1 - \frac{c}{c_0}) dt'$ (h)
0	0	1	2.000
2	0	1	0.995
3	0.01	0.99	0.975
4	0.04	0.96	0.930
$t_b \rightarrow 5$	0.10	0.90	4.900

So: $\int_0^{t_b} \left[1 - \frac{c(L,t)}{c_0} \right] dt = 4.900$ h,

and

$$\left(\frac{\text{mass solute}}{\text{area}} \right) \text{ adsorbed upto } t_b = (F_A)_{in} (4.900 \text{ h})$$

To get capacity in mass solute adsorbed/mass silica gel, use the fact that

$$\begin{aligned} \left(\frac{\text{mass silica gel}}{\text{area}} \right) &= \frac{\text{bed vol.}}{\text{bed area}} \cdot \frac{\text{mass silica gel}}{\text{bed vol.}} \\ &= L \rho_{bed} = (60 \text{ cm})(0.30 \frac{\text{g silica gel}}{\text{cm}^3}) \\ &= 18.0 \frac{\text{g silica gel}}{\text{cm}^2} \end{aligned}$$

Then

$$W_b = \frac{\text{mass adsorbed upto } t_b}{\text{mass silica gel}}$$

* Use trapezoid rule, $\int_a^b f(x) dx \approx \frac{b-a}{2} [f(a) + f(b)]$, for each interval

$$\begin{aligned}
 &= \frac{\text{mass adsorbed upto } t_b / \text{area}}{\text{mass silica gel / area}} \\
 W_b &= \frac{(F_A)_{in} (4.900 \text{ h})}{(L \rho_{bed})} = \frac{(0.352 \frac{\text{g solute}}{\text{cm}^2 \cdot \text{h}})(4.900 \text{ h})}{18.0 \frac{\text{g silica gel}}{\text{cm}^2}} \\
 &= 0.150 \frac{\text{g solute}}{\text{g silica gel}}
 \end{aligned}$$

Fraction of bed capacity used at break-point

$$= W_b / W_{sat} = 0.150 / 0.352 = 0.426$$

for 60 cm bed. Used length = $(0.426)(60 \text{ cm})$
 $= 25.6 \text{ cm}$

$$\text{Unused length} = (60 - 25.6) \text{ cm} = 34.4 \text{ cm}$$

Unused capacity of bed (in terms of equivalent bed length) at break-point is $l_{unused} = 34.4 \text{ cm}$

(c) Scale up principle — l_{unused} at t_b independent of bed length. For new longer bed,

$$l_{used} = L - l_{unused} = 100 \text{ cm} - 34.4 \text{ cm} = 65.6 \text{ cm}$$

$$\text{and } \frac{W_b}{W_{sat}} = \frac{l_{used}}{L} = \frac{65.6}{100}$$

Mass balance:

$$(F_A)_{in} A_c t_b - 0 = \underbrace{W_b}_{\substack{\text{mass solute} \\ \text{mass silica gel}}} \cdot \underbrace{L A_c \rho_{bed}}_{\substack{\text{mass silica} \\ \text{gel}}}$$

cross-sectional area of bed

(mass in upto t_b)

(mass solute / mass silica gel)

mass silica gel

Neglect solute out (very small and still only 0.150 at t_b).

Solve for t_b :

$$\begin{aligned} t_b &= \frac{W_b L A_c \rho_{bed}}{(F_A)_{in} A_c} \\ &= \left(\frac{W_b}{W_{total}} \right) W_{total} L \rho_{bed} \\ &= \frac{\left(\frac{65.6}{100} \right) \left(0.352 \frac{\text{g solids}}{\text{g solids}} \right) (100 \text{ cm}) \left(0.20 \frac{\text{g solids}}{\text{cm}^3} \right)}{0.552 \frac{\text{g solids}}{\text{cm}^2 \cdot \text{h}}} \end{aligned}$$

actually $\frac{W_b \cdot L}{W_{total}} = l_{used} = 65.6 \text{ cm}$

$$t_b = 12.5 \text{ h}$$

predicted break-point time
for 100 cm bed