

Problem 1

General $x_F = 0.65, x_D = 0.97, x_B = 0.025$

Feed line passes through pt. $(x_F, x_F) = (0.65, 0.65)$ and is horizontal (slope = 0) because feed is saturated vapor

(Not required: From graph on p. ②, $x_D / (R_{min} + 1) = 0.50 \Rightarrow$
 $R_{min} = 0.94$)

Part (a): R-up. line passes through pt $(x_D, x_D) = (0.97, 0.97)$ and has intercept $x_D / (R+1) = 0.30$.

S-op. line passes through pt. $(x_B, x_B) = (0.025, 0.025)$ and pt of intersecting of R-up + feed lines.

Draw effective equl. curve 3/4 of the way up from op. line to equl. curve because $\eta_m = 0.75$.

Stages: Do not use eff. equl. curve for 1st step, which represents partial condenser. Count steps thereafter, 4 do not use eff. equl. curve for last step, which represents reboiler. From graph on p. ②, need $\boxed{6}$ stages in the column itself. Feed stage is stage # 3.

perhaps 7 to be sure

Part (b): $D = F \left(\frac{x_F - x_B}{x_D - x_B} \right) = (20 \frac{\text{mol}}{\text{h}}) \left(\frac{0.65 - 0.025}{0.97 - 0.025} \right)$
 $= 52.9 \text{ mol/h}$

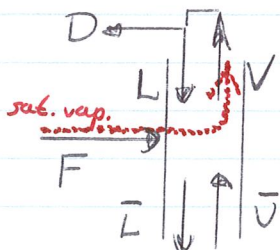
$R = \frac{L}{D} \Rightarrow L = RD = (2.23)(52.9) = 118.0 \text{ mol/h}$

$V = L + D = 170.9 \text{ mol/h}$

$V = \bar{V} + (1-q)F \Rightarrow \bar{V} = V - (1-q)F = V - F = \boxed{90.9 \text{ mol/h}}$

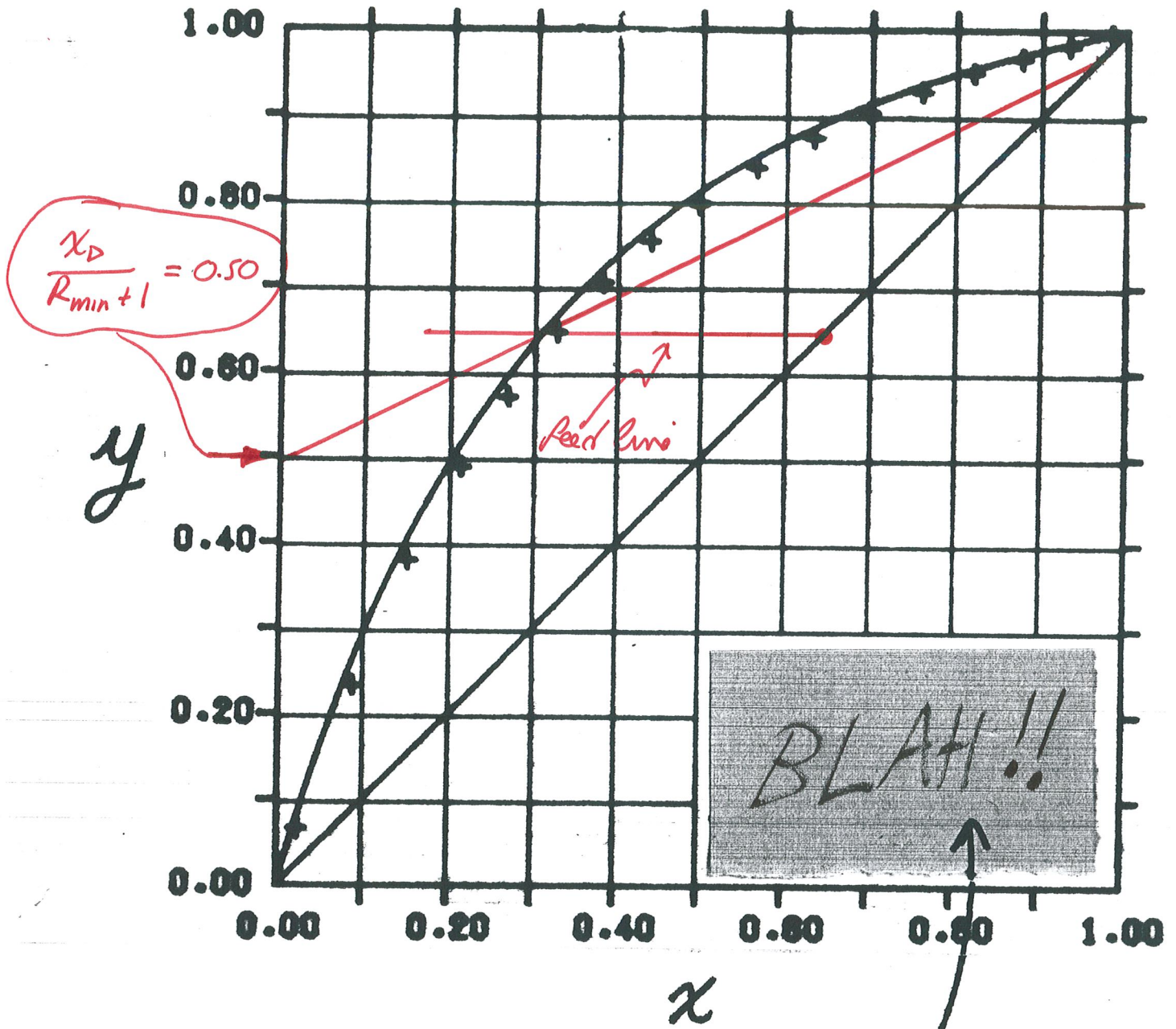
$R = L/D$

$\bar{L} = L + qF$



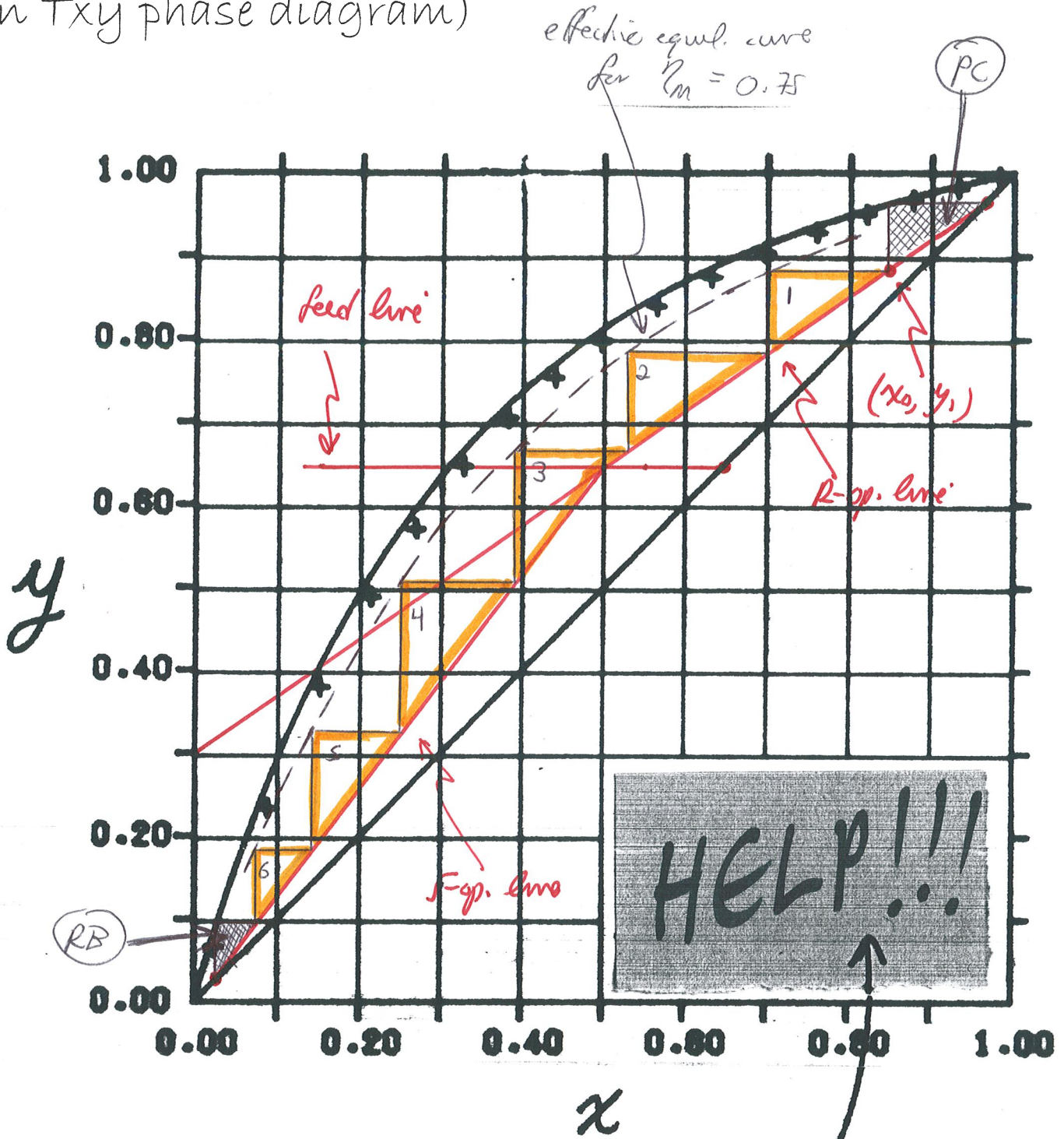
$V = \bar{V} + (1-q)F$

(Get xy pairs from a few horizontal lines drawn in Txy phase diagram)



(Get xy pairs from a few horizontal lines drawn in Txy phase diagram)

3



writing in this box is absolutely forbidden

Part (c): Enthalpy formula:

$$(H_y)_1 = 0 + 29,300 + 90(T-77)$$

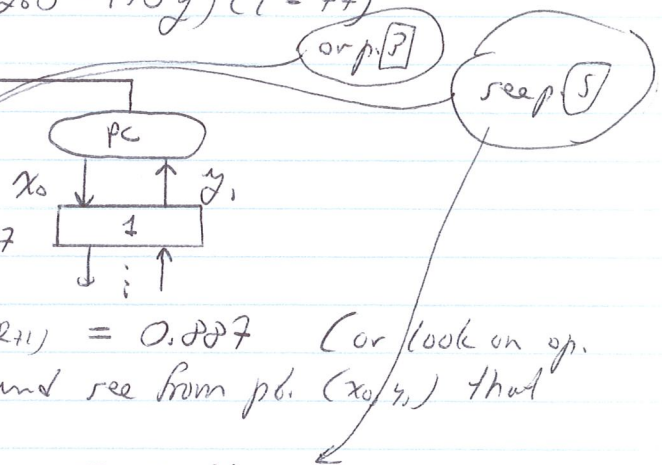
$$(H_y)_2 = 0 + \underbrace{(270)(125.5-77)}_{l, 77^\circ C \rightarrow 125.5^\circ C} + \underbrace{33,200}_{l \rightarrow v \text{ at } 125.5^\circ C} + \underbrace{260(77-125.5 + T-77)}_{v, 125.5^\circ C \rightarrow T}$$

$$= 34,205 + 260(T-77)$$

$$H_y = y(H_y)_1 + (1-y)(H_y)_2$$

$$= 34,205 - 4985y + (260 - 170y)(T-77)$$

Vapor entry PC: $x_D = y'$



$$y' = x_D = 0.97$$

$$x_0 = x \text{ in equl. w/ } y = 0.97 = 0.85$$

$$y_1 = [R/(R+1)]x_0 + x_D/(R+1) = 0.887 \text{ (or look on op. diagram (p. 3)) and see from pb. } (x_0, y_1) \text{ that } y_1 \approx 0.89.$$

Also, from T_{xy} phase diagram, $T_{y_1} \approx 80^\circ C$.

Enthalpy: With $y = 0.887$ and $T = 80^\circ C$, calculate

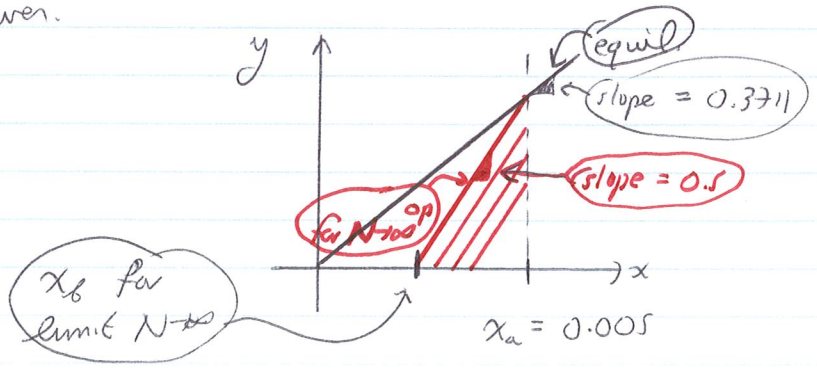
$$(H_{y_1}) = 31,065 \text{ J/mol}$$

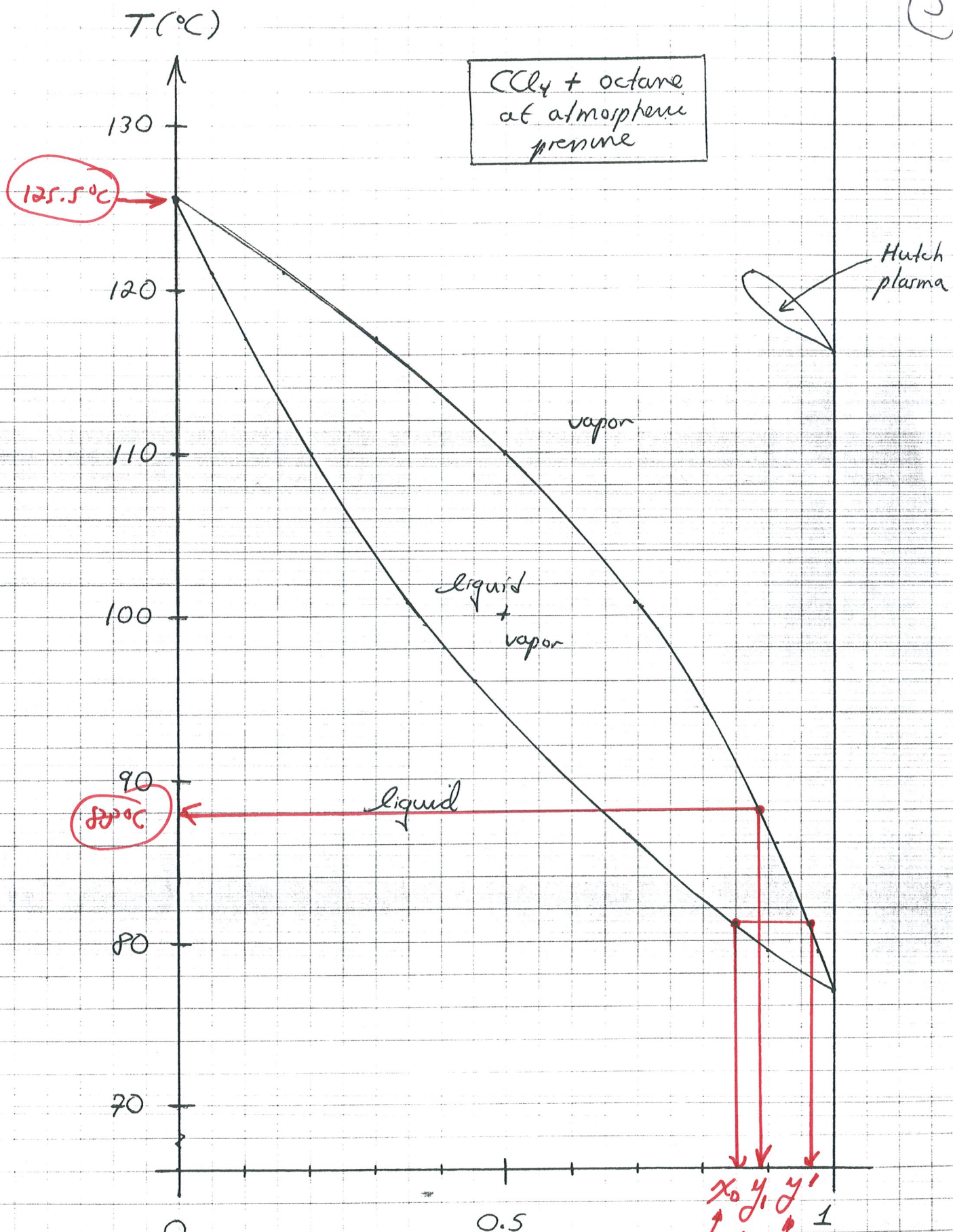
Problem 2

Henry's law const. for methanol

General: Equl. relation is $y = (k/P)x = (202/760)x = 0.3711x$

Part (a): Dilute solutions \Rightarrow op. line \approx straight line w/ slope $L/V \approx 9/18 = 0.5$. Slope of op. line $>$ slope of equl. curve. \therefore 1st contact as $N \rightarrow \infty$ occur @ a-end of tower.





Elroy-matic™ Data Sheet
No. 2

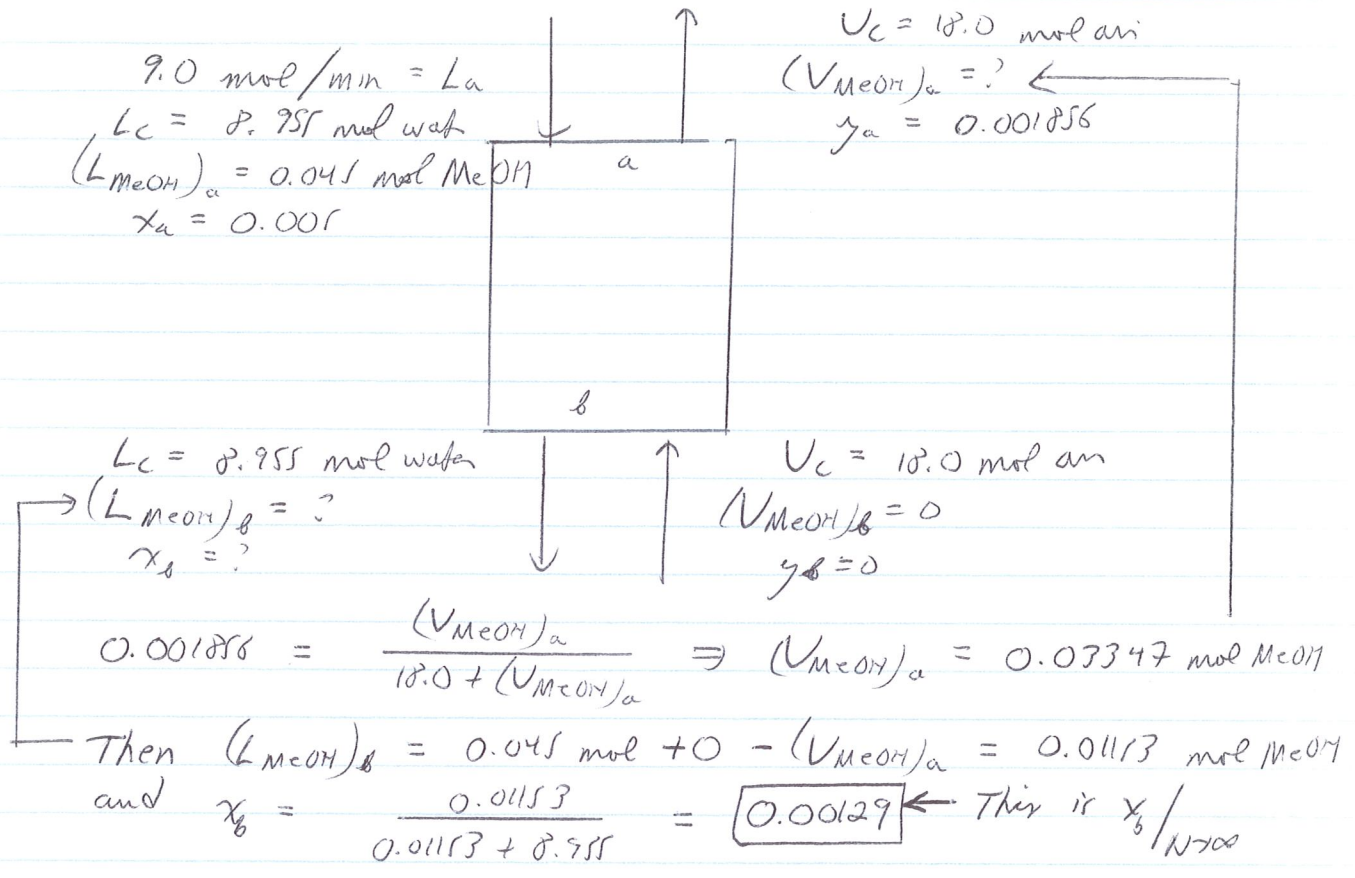
x, y

0.887

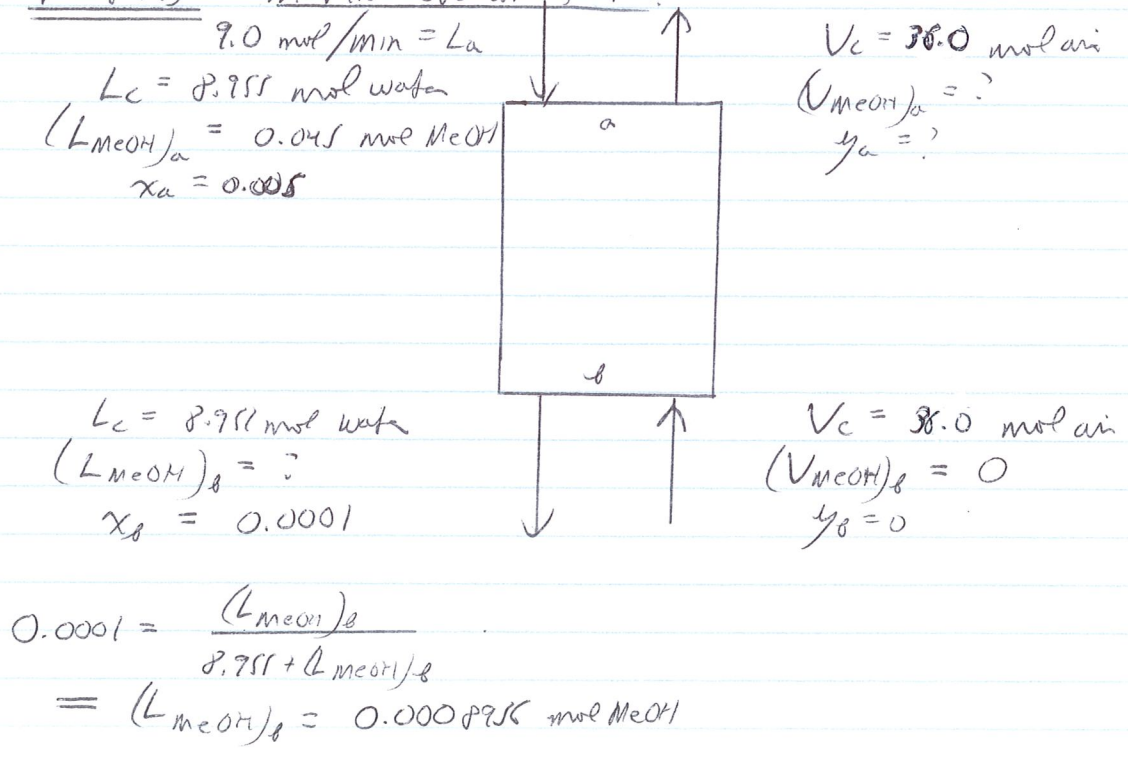
0.88

0.97

So: $y_a/N_{T,a} = (0.3711) x_a = 0.001856$ [$(x_a, y_a/N_{T,a})$ satisfies equl. relation]. Material balance for $N \rightarrow \infty$ works out as follows:



Part (b): Material balances, etc.:



(7)

$$\text{Then } (V_{\text{meq}})_a = 0.045 \text{ mol} + 0 - 0.0008956 \text{ mol} = 0.04410 \text{ mol}$$

$$\text{and } y_a = \frac{0.04410}{36.0 + 0.04410} = 0.001224$$

Kremser eq.:

$$y_a^* = y^*(x_a) = (0.3711)(0.005) = 0.001856$$

$$y_b^* = y^*(x_b) = (0.3711)(0.0001) = 0.00003711$$

$$N = \frac{\log\left(\frac{y_b - y_b^*}{y_a - y_a^*}\right)}{\log\left(\frac{y_b - y_b^*}{y_b^* - y_a^*}\right)} = \frac{\log\left(\frac{0 - 0.00003711}{0.001224 - 0.001856}\right)}{\log\left(\frac{0 - 0.001224}{0.00003711 - 0.001856}\right)}$$

$$= \boxed{7.16 \text{ stages} \Rightarrow 8 \text{ stages}}$$

Alternate Kremser eq.:

$$x_a^* = x^*(y_a) = \frac{y_a}{0.3711} = 0.003298$$

$$x_b^* = x^*(y_b) = \frac{y_b}{0.3711} = 0$$

$$N = \frac{\log\left(\frac{x_a - x_a^*}{x_b - x_b^*}\right)}{\log\left(\frac{x_a - x_b}{x_a^* - x_b^*}\right)} = \frac{\log\left(\frac{0.005 - 0.003298}{0.0001 - 0}\right)}{\log\left(\frac{0.005 - 0.0001}{0.003298 - 0}\right)}$$

$$= 7.16 \text{ stages (same answer)}$$